

Solving the advection PDE in explicit FTCS, Lax, Implicit FTCS and Crank-Nicolson methods for constant and varying speed.

Accuracy, stability and software animation

Report submitted for fulfillment of the Requirements for MAE 294
Masters degree project
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1 Introduction

The goal of this project is to analyze and compare different numerical methods for solving the first order advection PDE.

Following the analytical analysis for stability of the numerical scheme, animation were done to visually illustrate and confirm these results. This was carried for different parameters. The animation was programmed in Mathematica and saved to animated gif files which was then loaded into the HTML version of this report located here .

Fortran 95 was used for the computation part, while Mathematica was used for the animation and graphics part.

The above link contains all the supporting material for the project, including the Fortran program (in source and windows executable format) used to carry the main computation, and the Mathematica program used to do the animation and the Unix bash file used to process the computation for different parameters.

The specific PDE example used for the analysis and animation was the one provided by Professor Donald Dabdub for the final exam for his MAE 185 course (Numerical methods for mechanical engineers) in spring 2006. This PDE is described below:

Solve numerically

$$\frac{\partial c}{\partial t} + u \frac{\partial c}{\partial x} = 0$$

Where $c(x, t)$ is the concentration of a given material as a function of time and space.

The above is solved for the following 2 cases

1. u (the advection speed, or the speed at which the mass is being transported) is a constant value given as (2 ft/min).
2. u is a function of time defined as $u(t) = \frac{t}{20}$ ft/min

The problem parameters are:

$$\begin{aligned} t &\geq 0 \\ 0 &\leq x \leq L \end{aligned}$$

Where $L = 100$ feet.. Initial conditions are

$$c(x, 0) = F(x) = \begin{cases} 1 + \cos\left(\pi\left(\frac{x-30}{5}\right)\right) & 25 \leq x \leq 25 \\ 0 & \text{otherwise} \end{cases}$$

The boundary conditions are

$$\begin{aligned} c(0, t) &= 0 \\ c(L, t) &= 0 \end{aligned}$$

This PDE is an example of an IBVP (Initial and Boundary Value Problem).

Different numerical methods are used to solve the above PDE. The methods are compared for stability using Von Neumann stability analysis.

The numerical methods are also compared for accuracy. This was done by comparing the numerical solution to the known analytical solution at each time step. The comparison was done by computing the root mean square error (RMSE) between the numerical and the analytical solution at each time step.

The method with the least RMSE at the end of the simulation is considered the most accurate.

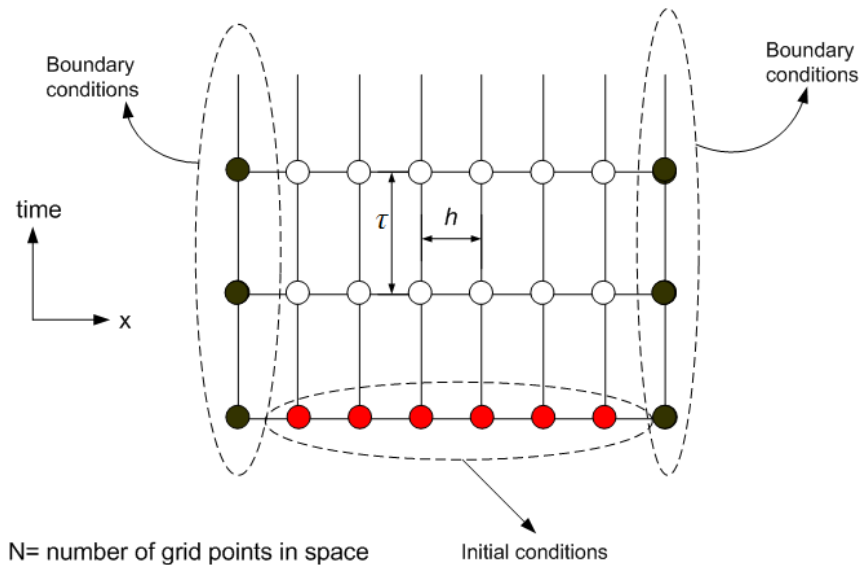
The above PDE has a known analytical solution which is

$$C(x, t) = F(x - ut)$$

The above analytical solution indicates that the initial concentration will move from left to right with the advection speed u .

The formulation of each numerical method is shown below. h is used to represent Δx , the space between 2 space grid point, or the space step size, and τ is used to represent Δt , the time step.

The space line has N grid points. The spacing h was fixed at 0.01 ft for all the methods and for all the test cases, while τ was changed. This made comparing the different methods simpler. The following diagram illustrates the discretization used.



Should we consider the lower left and the lower right grid points above as part of the initial conditions, or part of the boundary conditions?

Stability of each method is derived. Stability is important, since by the Lax-Richtmyer equivalence theorem¹, stability implies convergence of the solution. Convergence of the numerical solutions implies that as the step size becomes smaller, the numerical solution converges to the analytical solution.

Explicit and implicit numerical methods are used. When solving for the future value of the solution at a single node in terms of only past values, the method is called an explicit method. In other words, when the only unknown is the future value of the solution at a single node, and everything else on the right hand side of the finite difference equation is a solution derived at earlier time step, the method is explicit.

An implicit method is one in which the finite difference equation contains the solution at a at future time at more than one node. In other words, future solution are being solved for at more than one node in terms of the solution at earlier time. Implicit methods therefor are usually solved by matrix methods by solving $Ax = b$ where b represents present present known solution values, and x are the unknown future solution values, and A is the coefficient matrix which will usually be block diagonal (or tri diagonal) in shape.

In the derivations below, the notation of C_i^n is used to indicate the solution at time step n and at space node i . Hence $C(x_i, t_n)$ is written as C_i^n . This notation seems to be more clear than the $C_{i,n}$ notation.

Different finite difference schemes for solving a PDE are obtained by using different methods of approximating the derivative terms in the PDE.

This will be illustrated using the space derivative $\frac{\partial c}{\partial x}$. This derivative can be approximated in one of the following 3 ways (all at time step n)

1.1 Backward difference (Upwind)

$$\frac{\partial c}{\partial x} \approx \frac{C_i^n - C_{i-1}^n}{h}$$

¹Richtmyer and Morton 1967. p45): "Given a properly posed linear initial value problem and a finite difference approximation to it that satisfies the consistency condition, stability is the necessary and sufficient condition for convergence."

1.2 Forward difference (downwind)

$$\frac{\partial c}{\partial x} \approx \frac{C_{i+1}^n - C_i^n}{h}$$

1.3 Center difference

$$\frac{\partial c}{\partial x} \approx \frac{C_{i+1}^n - C_{i-1}^n}{2h}$$

The following are the derivation of a number of methods for solving the advection PDE obtained by using the above definitions for the derivative when applied to both space and time.

2 Numerical schemes

2.1 Explicit Methods

2.1.1 FTCS

With FTCS, the forward time derivative, and the centered space derivative are used. Hence the advection PDE can be written as

$$\frac{C_i^{n+1} - C_i^n}{\tau} = -u \left(\frac{C_{i+1}^n - C_{i-1}^n}{2h} \right) \quad (0)$$

Solving for C_i^{n+1} results in

$$\boxed{C_i^{n+1} = C_i^n - \frac{u\tau}{2h} (C_{i+1}^n - C_{i-1}^n)} \quad (1)$$

This method will be shown to be unconditionally unstable.

2.1.2 Downwind

Here, the forward time derivative for $\frac{\partial C}{\partial t}$ is used and also the forward space derivative for $\frac{\partial C}{\partial x}$. This results in

$$\frac{C_i^{n+1} - C_i^n}{\tau} = -u \left(\frac{C_{i+1}^n - C_i^n}{h} \right)$$

$$\boxed{C_i^{n+1} = C_i^n - \frac{u\tau}{h} (C_{i+1}^n - C_i^n)}$$

This method will be shown to be unconditionally unstable as well.

2.1.3 Upwind

Here, the forward time derivative for $\frac{\partial C}{\partial t}$ is used, and the backward derivative for $\frac{\partial C}{\partial x}$ is used. This results in

$$\frac{C_i^{n+1} - C_i^n}{\tau} = -u \left(\frac{C_i^n - C_{i-1}^n}{h} \right)$$

$$\boxed{C_i^{n+1} = C_i^n - \frac{u\tau}{h} (C_i^n - C_{i-1}^n)}$$

This will be shown to be stable if $\frac{u\tau}{h} \leq 1$

2.1.4 LAX

Looking at the FTCS eq (1) above, and shown below again

$$C_i^{n+1} = C_i^n - \frac{u\tau}{2h} (C_{i+1}^n - C_{i-1}^n)$$

The term C_i^n above is replaced by its average value $\frac{C_{i+1}^n + C_{i-1}^n}{2}$ to obtain the LAX method

$$\boxed{C_i^{n+1} = \frac{1}{2} (C_{i+1}^n + C_{i-1}^n) - \frac{u\tau}{2h} (C_{i+1}^n - C_{i-1}^n)} \quad (4)$$

This method will be shown to be stable if $\frac{u\tau}{h} \leq 1$

2.1.5 Lax-Wendroff

By using the second-order finite difference scheme for the time derivative, the method of Lax-Wendroff method is obtained

$$C_i^{n+1} = C_i^n - \frac{u\tau}{2h} (C_{i+1}^n - C_{i-1}^n) + \frac{u^2\tau^2}{2h^2} (C_{i+1}^n + C_{i-1}^n - 2C_i^n)$$

2.1.6 Leap-frog

In this method, the centered derivative is used for both time and space. This results in

$$\boxed{\frac{C_i^{n+1} - C_i^{n-1}}{2\tau} = -u \left(\frac{C_{i+1}^n - C_{i-1}^n}{2h} \right)}$$

This method requires a special starting procedure due to the term C_i^{n-1} . Another scheme such as Lax can be used to kick start this method.

2.2 Implicit Methods

2.2.1 Implicit FTCS

Given the explicit FTCS derived above

$$\frac{C_i^{n+1} - C_i^n}{\tau} = -u \left(\frac{C_{i+1}^n - C_{i-1}^n}{2h} \right)$$

The above is modified it by evaluating the space center derivative at time step $n + 1$ instead of at time step n , this results in

$$\frac{C_i^{n+1} - C_i^n}{\tau} = -u \left(\frac{C_{i+1}^{n+1} - C_{i-1}^{n+1}}{2h} \right) \quad (5A)$$

Hence

$$\boxed{C_i^{n+1} + \frac{u\tau}{2h} C_{i+1}^{n+1} - \frac{u\tau}{2h} C_{i-1}^{n+1} = C_i^n} \quad (5B)$$

Writing it in matrix form, first letting $\alpha = \frac{u\tau}{2h}$ results in

$$\begin{bmatrix} 1 & 0 & 0 & 0 & \cdots & 0 & 0 \\ -\alpha & 1 & \alpha & 0 & \cdots & 0 & 0 \\ 0 & -\alpha & 1 & \alpha & \cdots & 0 & 0 \\ 0 & 0 & -\alpha & 1 & \alpha & \cdots & 0 \\ \vdots & & & & & & \\ 0 & 0 & 0 & 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} C_0^{n+1} \\ C_1^{n+1} \\ C_2^{n+1} \\ C_3^{n+1} \\ \vdots \\ C_{N-1}^{n+1} \end{bmatrix} = \begin{bmatrix} C_0^n \\ C_1^n \\ C_2^n \\ C_3^n \\ \vdots \\ C_{N-1}^n \end{bmatrix}$$

Where N is the number of space grid points.

The above is written as

$$Ax = b$$

Solving for x , which represents the solution at time step $n + 1$ or at time $t = (n + 1)\tau$. b represents the current solution at time step n , and A is the matrix of the coefficients shown above.

Due to the form of the A matrix, (Called tri diagonal, or Block diagonal), an algorithm that takes advantages of this form is used. This is called the Thomas algorithm. This greatly speeds up the solution. If we had used a general algorithm to solve this system such as the Gauss elimination method, it would have been much slower,

making the implicit method not practical to use. (Some tests on the same data showed the Thomas algorithm to be 50 times faster than Gaussian elimination).

2.2.2 Wendrof

This method uses center difference for the derivative around the space step $(i + \frac{1}{2})h$ and the time step $(n + \frac{1}{2})\tau$. This leads to the following scheme

$$\boxed{\left(1 - \frac{u\tau}{h}\right) C_i^{n+1} + \left(1 + \frac{u\tau}{h}\right) C_{i+1}^{n+1} = \left(1 + \frac{u\tau}{h}\right) C_i^n + \left(1 - \frac{u\tau}{h}\right) C_{i+1}^n}$$

This can also be solved using similar matrix method to that used for the implicit FTCS. This method is not used in this report.

2.2.3 Crank-Nicolson

By taking the average of the explicit FTCS and the implicit FTCS formulations (shown again below), the C-N scheme is derived

$$\frac{C_i^{n+1} - C_i^n}{\tau} = -u \left(\frac{C_{i+1}^n - C_{i-1}^n}{2h} \right)$$

$$\frac{C_i^{n+1} - C_i^n}{\tau} = -u \left(\frac{C_{i+1}^{n+1} - C_{i-1}^{n+1}}{2h} \right)$$

Taking the average of the above results in

$$\frac{C_i^{n+1} - C_i^n}{\tau} = -\frac{u}{2} \left(\frac{C_{i+1}^n - C_{i-1}^n}{2h} \right) - \frac{u}{2} \left(\frac{C_{i+1}^{n+1} - C_{i-1}^{n+1}}{2h} \right)$$

$$\boxed{C_i^{n+1} + \frac{u\tau}{4h} C_{i+1}^{n+1} - \frac{u\tau}{4h} C_{i-1}^{n+1} = C_i^n - \frac{u\tau}{4h} C_{i+1}^n + \frac{u\tau}{4h} C_{i-1}^n}$$

Now the system $Ax = b$ is setup to solve for future values as follows. Let $\alpha = \frac{u\tau}{4h}$, the system can be written as

$$\begin{bmatrix} 1 & 0 & 0 & 0 & 0 & 0 \\ -\alpha & 1 & \alpha & 0 & 0 & 0 \\ 0 & -\alpha & 1 & \alpha & 0 & 0 \\ 0 & 0 & -\alpha & 1 & \alpha & 0 \\ 0 & 0 & 0 & -\alpha & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 \end{bmatrix} \begin{bmatrix} C_0^{n+1} \\ C_1^{n+1} \\ C_2^{n+1} \\ C_3^{n+1} \\ \vdots \\ C_{N-1}^{n+1} \end{bmatrix} = \begin{bmatrix} C_0^n \\ C_1^n - \alpha C_2^n + \alpha C_0^n \\ C_2^n - \alpha C_3^n + \alpha C_1^n \\ C_3^n - \alpha C_4^n + \alpha C_2^n \\ \vdots \\ C_{N-1}^n \end{bmatrix}$$

Thomas algorithm is used to solve the above system for C_i^{n+1} .

3 Stability analysis

A numerical solution is stable if the "energy content" remain below some limiting value no matter how long the solution is integrated. In essence, this means that the solution does not 'blow up' after some time. This can be called BIBO stability (Bounded In Bounded Out).

Hence one way to analyze the stability of the numerical solution is to determine an expression that relates the amplitude of the solution between 2 time steps, and to determine if this ratio remain less than or equal to a unity as more and more time steps are taken.

This type of analysis is called Von Neumann stability analysis for numerical methods.

The analysis is based of finding an expression for the magnification factor of the wave amplitude at each step. The solution will be stable if this magnification factor is less than one.

Let the magnification factor be ζ . The numerical scheme is stable iff

$$|\zeta| \leq 1$$

The Courant–Friedrichs–Lewy (CFL) criteria for stability says that

$$|\zeta| \leq 1 \Leftrightarrow \left| \frac{u\tau}{h} \right| \leq 1$$

Where u , h , and τ are as defined above: u is the wave speed, $h = \Delta x$ and $\tau = \Delta t$.

The number $\frac{u\tau}{h}$ is also called the courant number.

Some numerical methods will be shown to be unconditionally unstable (such as explicit FTCS and the explicit upwind). This means that even if courant number was ≤ 1 , the numerical solutions will eventually become unstable.

Some explicit methods such as LAX, are conditionally stable if the courant number was ≤ 1 .

Implicit methods are unconditionally stable, hence courant number is not used for these methods. However, this does not mean one can take as large step as one wants with the implicit methods, since accuracy will be affected even if the solution remain stable.

Hence, the best numerical scheme is one in which the largest step size can be taken, with the least amount of inaccuracy in the numerical solution while remaining stable.

For numerical scheme that are conditionally stable, it can be seen from the CFL condition that for a fixed speed u and fixed h , the maximum time step that can be taken is given by

$$\tau_{\max} \leq \frac{h}{u}$$

It can be immediately seen from above, that for the case when the advection speed is varying and is a function of time such as the case when $u(t) = \frac{t}{20}$ implying that the speed is increasing with time, then when using a fixed time step τ it will eventually become larger than $\frac{h}{u}$ and the numerical scheme will be unstable. This is because as $u(t)$ is becoming larger and larger, while h is fixed, the term $\frac{h}{u}$ will become smaller and smaller.

Hence to keep the courant number $\frac{u\tau}{h} \leq 1$, the time step taken must remain less than $\frac{h}{u}$, hence using a fixed time step with increasing u will eventually lead to instability.

This will affect the explicit methods that are conditionally stable such as the LAX method, since the Lax method is explicit and depends on satisfying the CFL all the time for its stability. Implicit methods are stable for any time step.

In the following we derive the details of the stability analysis and use Von Neumann analysis to derive an expression for the amplification factor ζ for different numerical schemes.

So to summarize:

1. Explicit FTCS is unconditionally unstable.
2. Explicit LAX is stable if $\frac{u\tau}{h} \leq 1$, or in other words, $\tau_{\max} \leq \frac{h}{u}$
3. Implicit FTCS and C-R are stable for all τ

3.1 Stability analysis for FTCS

Using Von Neumann method, the following trial solution to the PDE is assumed

$$c(x, t) = A(t) e^{jkx}$$

where $j = \sqrt{-1}$ and k is the wave number and A is the amplitude of the wave, as a function of time.

Hence the solution at time step n and at $x = x_i = ih$ is written as

$$A^n e^{jkih} \tag{2}$$

Substitute this trial solution (2) into the (1) results in

$$A^{n+1} e^{jkih} = A^n e^{jkih} - \frac{u\tau}{2h} \left(A^n e^{jk(i+1)h} - A^n e^{jk(i-1)h} \right) \tag{3}$$

Let ξ be the ratio of the amplitude of the wave at time step $n + 1$ relative to that at time step n . hence

$$\xi = \frac{A^{n+1}}{A^n}$$

Divide (3) by A^n results in

$$\xi e^{jkih} = e^{jkih} - \frac{u\tau}{2h} \left(e^{jk(i+1)h} - e^{jk(i-1)h} \right)$$

Divide the above by e^{jkih}

$$\begin{aligned} \xi &= 1 - \frac{u\tau}{2h} \left(e^{jkh} - e^{-jkh} \right) \\ &= 1 - \frac{u\tau}{h} j \sin(kh) \end{aligned}$$

Hence

$$|\xi| = \sqrt{1 + \left(\frac{u\tau}{h} \sin(kh) \right)^2}$$

This implies that $|\xi| \geq 1$ regardless of the time step τ selected or the space step h , hence

FTCS is unconditionally unstable.

For a fixed speed u , the instability can be delayed by making $\frac{\tau}{h}$ smaller, but it could not be prevented. Eventually this numerical solution will blow up. This will be illustrated below in an animation. See case 3 and 4 as examples.

The instability can be delayed by making τ smaller for a fixed h , or by making h larger for a fixed τ .

3.2 Stability analysis of the downwind method

$$C_i^{n+1} = C_i^n - \frac{u\tau}{h} (C_{i+1}^n - C_i^n)$$

Substitute the trial solution $A^n e^{jkih}$ into the above

$$\begin{aligned} A^{n+1} e^{jkih} &= A^n e^{jkih} - \frac{u\tau}{h} \left(A^n e^{jk(i+1)h} - A^n e^{jk(i-1)h} \right) \\ \xi &= 1 - \frac{u\tau}{h} \left(e^{jkh} - 1 \right) \\ &= 1 + \frac{u\tau}{h} - \frac{u\tau}{h} e^{jkh} \\ &= 1 + \frac{u\tau}{h} - \frac{u\tau}{h} (\cos(kh) + j \sin(kh)) \\ &= 1 + \frac{u\tau}{h} (1 - \cos kh) - j \frac{u\tau}{h} \sin kh \end{aligned}$$

Let $\frac{u\tau}{h} = \lambda$
Hence

$$\xi = 1 + \lambda(1 - \cos kh) - j\lambda \sin kh$$

$$\begin{aligned} |\xi|^2 &= (1 + \lambda(1 - \cos kh))^2 + (\lambda \sin kh)^2 \\ &= 1 + 2\lambda(1 - \cos kh) + \lambda^2(1 - \cos kh)^2 + \lambda^2 \sin^2 kh \\ &= 1 + 2\lambda(1 - \cos kh) + \lambda^2(1 - 2\cos kh + \cos^2 kh) + \lambda^2 \sin^2 kh \\ &= 1 + 2\lambda - 2\lambda \cos kh + \lambda^2 - 2\lambda^2 \cos kh + \lambda^2 \cos^2 kh + \lambda^2 \sin^2 kh \\ &= 1 + 2\lambda - 2\lambda \cos kh + 2\lambda^2 - 2\lambda^2 \cos kh \\ &= 1 + 2\lambda(1 + \lambda)(1 - \cos kh) \end{aligned}$$

Hence for stability it is required that

$$|1 + 2\lambda(1 + \lambda)(1 - \cos kh)| \leq 1$$

or

$$2\lambda(1 + \lambda)(1 - \cos kh) \leq 0$$

since $\lambda = \frac{u\tau}{h}$, a positive quantity, then the above condition can not be satisfied. Hence the downwind method is unconditionally unstable.

3.3 Stability analysis of the upwind method

$$C_i^{n+1} = C_i^n - \frac{u\tau}{h} (C_i^n - C_{i-1}^n)$$

Substitute the trial solution $A^n e^{jkih}$ into the above

$$\begin{aligned} A^{n+1} e^{jkih} &= A^n e^{jkih} - \frac{u\tau}{h} (A^n e^{jkih} - A^n e^{jk(i-1)h}) \\ \xi &= 1 - \frac{u\tau}{h} (1 - e^{-jkh}) \\ &= 1 - \frac{u\tau}{h} + \frac{u\tau}{h} e^{-jkh} \\ &= 1 - \frac{u\tau}{h} + \frac{u\tau}{h} (\cos(kh) - j \sin(kh)) \\ &= 1 - \frac{u\tau}{h} (1 - \cos kh) - j \frac{u\tau}{h} \sin kh \end{aligned}$$

Let $\frac{u\tau}{h} = \lambda$
Hence

$$\xi = 1 - \lambda(1 - \cos kh) - j\lambda \sin kh$$

Hence

$$\begin{aligned} |\xi|^2 &= (1 - \lambda(1 - \cos kh))^2 + (\lambda \sin kh)^2 \\ &= 1 - 2\lambda(1 - \cos kh) + \lambda^2(1 - \cos kh)^2 + \lambda^2 \sin^2 kh \\ &= 1 - 2\lambda + 2\lambda \cos kh + \lambda^2(1 + \cos^2 kh - 2\cos kh) + \lambda^2 \sin^2 kh \\ &= 1 - 2\lambda + 2\lambda \cos kh + \lambda^2 + \lambda^2 \cos^2 kh - 2\lambda^2 \cos kh + \lambda^2 \sin^2 kh \\ &= 1 - 2\lambda + 2\lambda \cos kh + 2\lambda^2 - 2\lambda^2 \cos kh \\ &= 1 - 2\lambda(1 - \lambda)(1 - \cos kh) \end{aligned}$$

Hence for stability it is required that

$$|1 - 2\lambda(1 - \lambda)(1 - \cos kh)| \leq 1$$

or

$$-2\lambda(1 - \lambda)(1 - \cos kh) \leq 0$$

Which will be true only if $(1 - \lambda) \geq 0$ or $\lambda \leq 1$ hence this implies

$$\frac{u\tau}{h} \leq 1$$

Hence the upwind method is stable if the CFL condition is satisfied. This will be seen as the same stability condition for the Lax method below.

3.4 Stability analysis of Lax

Replace the trial function from (2) in Lax formulation in (4) and obtain

$$A^{n+1}e^{jkih} = \frac{1}{2} \left(A^n e^{jk(i+1)h} + A^n e^{jk(i-1)h} \right) - \frac{u\tau}{2h} \left(A^n e^{jk(i+1)h} - A^n e^{jk(i-1)h} \right)$$

Divide by $A^n e^{jkih}$, the magnification factor ζ is obtained

$$\begin{aligned} \zeta &= \frac{1}{2} \left(e^{jkh} + e^{-jkh} \right) - \frac{u\tau}{2h} \left(e^{jkh} - e^{-jkh} \right) \\ &= \cos(kh) - j \frac{u\tau}{h} \sin(kh) \end{aligned}$$

Hence

$$|\zeta| = \sqrt{\cos^2(kh) + \left(\frac{u\tau}{h} \right)^2 \sin^2(kh)}$$

Since $\cos^2(kh) \leq 1$ and $\sin^2(kh) \leq 1$, then it is seen that $|\zeta| \leq 1$ if $\frac{u\tau}{h} \leq 1$

Hence the following is the condition for stability

$$\tau \leq \frac{h}{u}$$

As mentioned earlier, this is called the CFL condition.

The Lax method is stable for $\tau \leq \frac{h}{u}$ however, a modified version of this method is more accurate, which is the Lax-Wendroff method.

3.5 Stability of Lax-Wendroff

This is the same as the Lax method. The method is stable if $\tau \leq \frac{h}{u}$

3.6 Stability analysis of the Implicit FTCS

Replace the trial function from (2) in (5B) results in

$$A^{n+1}e^{jkih} + \frac{u\tau}{2h} A^{n+1}e^{jk(i+1)h} - \frac{u\tau}{2h} A^{n+1}e^{jk(i-1)h} = A^n e^{jkih}$$

Divide by $A^n e^{jkih}$

$$\begin{aligned}
\xi + \frac{u\tau}{2h}\xi e^{jkh} - \frac{u\tau}{2h}\xi e^{-jkh} &= 1 \\
\xi \left(1 + \frac{u\tau}{2h}e^{jkh} - \frac{u\tau}{2h}e^{-jkh}\right) &= 1 \\
\xi \left(1 + j\frac{u\tau}{h}\sin(kh)\right) &= 1 \\
\xi &= \frac{1}{1 + j\frac{u\tau}{h}\sin(kh)} = \frac{1 - j\frac{u\tau}{h}\sin(kh)}{1 + \frac{u\tau}{h}\sin(kh)}
\end{aligned}$$

Hence

$$|\xi| = \frac{\sqrt{1 + \left(\frac{u\tau}{h}\right)^2 \sin^2(kh)}}{1 + \frac{u\tau}{h}\sin(kh)} < 1$$

Hence this shows that the

Implicit FTCS method is unconditionally stable.

This property is common to all implicit methods.

Even though the implicit FTCS is stable, it is not very accurate. See case 8 below for an example.

4 Solution Results and Output

For the Fortran implementation, the following methods are implemented. The explicit FTCS, Explicit Lax, Implicit FTCS, and Implicit Crank-Nicolson.

For each method, the following was generated

1. CPU time used for the run.
2. snap shot of the solution at $t = 0, t = 15$, and $t = 30$ minutes.
3. RMSE between the numerical solution and the analytical solution.
4. Animation of the numerical solution. The animation was done by taking snapshots of the solution at regular intervals in Fortran. These were saved to disk. Then Mathematica was used to generate the animation and the plots.

To compare the stability and accuracy of the methods, the time step was changed (increased) and a new run was made. 8 different values of time steps are used. So there are 8 tests cases. These 8 test cases were run for both fixed speed ($u = 2$ ft/min) and for $u = \frac{t}{20}$ ft/min.

This table below summarizes these cases. The appendix contains all the plots. The animations are added as HTML links.

4.1 Case 1

$\tau = 0.0001$ sec, $h = 0.1$ ft

Speed	Method	CPU time (sec)	RMSE	Animation (2D)	plots
U=2	Explicit FTCS	20	0.0546		
	Explicit LAX	31	0.0543		
	Implicit FTCS	45	0.0548		
	C-R	49	0.0544		
U=t/20	Explicit FTCS	21	0.003		
	Explicit LAX	31	0.0031		
	Implicit FTCS	67	0.0031		
	C-R	69	0.0032		

Note the following: The explicit FTCS remained stable throughout the run due to the small time step. All other methods were stable as well during the run. For the CPU for the varying u case, notice that for the implicit methods this value is larger than the CPU for the same methods but when u is fixed. This is due to the fact that the matrix A is no longer constant, and must be recomputed at each time step before calling Thomas algorithm to solve $Ax = b$ system.

Also notice that the CPU time for the implicit methods is larger than the explicit methods. This is due to the extra computational cost in solving $Ax = b$. Even when using Thomas algorithm, this is still more expensive than the explicit methods when number of time steps is large.

4.2 Case 2

$\tau = 0.001$ sec, $h = 0.1$ ft

Speed	Method	CPU time (sec)	RMSE	Animation (2D)	plots
U=2	Explicit FTCS	2.42	0.01264		
	Explicit LAX	3.48	0.0057		
	Implicit FTCS	4.7	0.00742		
	C-R	4.9	0.00575		
U=t/20	Explicit FTCS	2.5	0.00352		
	Explicit LAX	3.5	0.00329		
	Implicit FTCS	7	0.00337		
	C-R	7.5	0.0033		

The explicit FTCS is stable for most of the run, near the end it is starting to be become unstable.

Notice that around 26 minutes that "bubbles" are starting to show up in the numerical solution downstream. This is a characteristic of how this method becomes unstable.

This will be more clear in the next test cases when the time step is made larger. For the varying speed case, the explicit method using the same time step remained stable during the whole 30 minutes. This is because the average speed was less than 2 ft/min, hence the mass did not have to travel as long a distance as with fixed speed of $u = 2$, and so the instability did not show up. Mathematically this can be explained by looking at the term $\frac{u\tau}{h}$, hence for smaller u , the courant number is smaller. Notice also the RMSE is smaller for variable speed compared to fixed speed. Again this is related to the smaller average speed making the courant number smaller.

4.3 Case 3

In this case, we slightly make the time step longer than before. We start to see the instability of FTCS.

$\tau = 0.0013$ sec, $h = 0.1$ ft, $\frac{u\tau}{h} = 0.026 \leq 1$ for fixed u

Speed	Method	CPU time (sec)	RMSE	Animation (2D)	plots
U=2	Explicit FTCS	1.9	0.0494		
	Explicit LAX	2.78	0.01125		
	Implicit FTCS	3.7	0.01245		
	C-R	3.9	0.01128		
U=t/20	Explicit FTCS	2.0	0.00365		
	Explicit LAX	2.9	0.00331		
	Implicit FTCS	5.56	0.00346		
	C-R	6	0.00331		

For explicit FTCS, The solution now starting to show instability at 25 minutes. Lax remained stable since CFL is satisfied. Explicit FTCS is becoming less accurate as well. Explicit Lax is most accurate at this time step.

4.4 Case 4

In this case, we slightly make the time step even longer than before. Now FTCS becomes more unstable.

$\tau = 0.0015$ sec, $h = 0.1$ ft, $\frac{u\tau}{h} = 0.03 \leq 1$.

Speed	Method	CPU time (sec)	RMSE	Animation (2D)	plots
U=2	Explicit FTCS	1.73	0.15249		
	Explicit LAX	2.56	0.000563		
	Implicit FTCS	3.34	0.009005		
	C-R	3.45	0.00565		
U=t/20	Explicit FTCS	1.84	0.00380		
	Explicit LAX	2.53	0.00336		
	Implicit FTCS	4.73	0.00358		
	C-R	5	0.003373		

FTCS Instability starts at around 20 minutes. LAX remained stable since CFL is satisfied. Lax remained the most accurate at this time step. Its accuracy actually improved as the time step became larger.

4.5 case 5

Again the time step is made longer than before. Now the explicit FTCS is completely unstable.

$$\tau = 0.045 \text{ sec}, h = 0.1 \text{ ft}$$

For the case of fixed U , we have $\frac{u\tau}{h} = \frac{2 \times 0.045}{0.1} = 0.9 \leq 1$, while for varying U , the maximum value will be at the end of the run, which is $30/20 = 1.5 \text{ ft/min.}$, hence the CFL condition is changing, with a value of $\frac{1.5 \times 0.045}{0.1} = 0.675$ at the end of the run which is still ≤ 1

Speed	Method	CPU time (sec)	RMSE	Animation (2D)	plots
U=2	Explicit FTCS	0.73	blows up		
	Explicit LAX	0.281	0.000162		
	Implicit FTCS	0.437	0.1306		
	C-R	0.4	0.01028		
U=t/20	Explicit FTCS	0.28	blow up		
	Explicit LAX	0.3	0.01117		
	Implicit FTCS	0.40	0.0386		
	C-R	0.4	0.01197		

For the varying speed case, the explicit FTCS remained stable for the duration of the run as compared to the case with the fixed speed. This is because the average wave speed is less than with the fixed wave speed case.

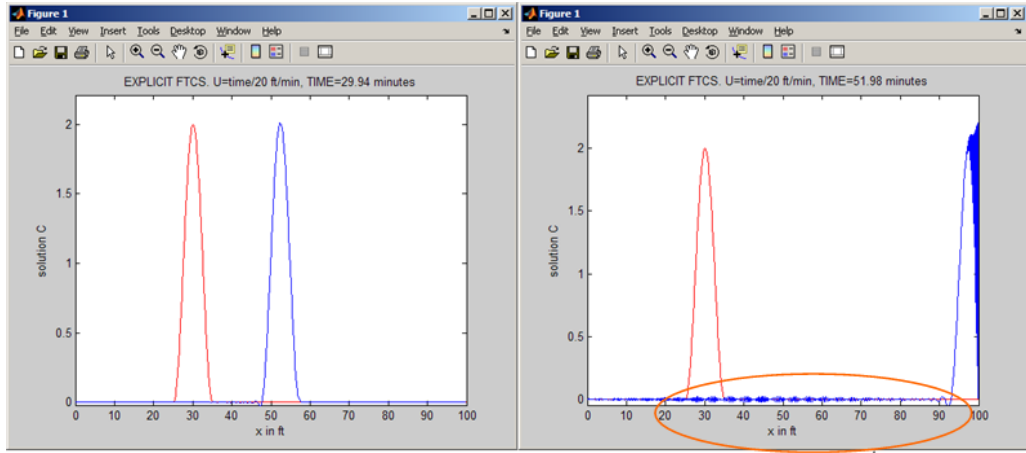
The magnification factor depends on the speed of the wave.

$$|\xi| = \sqrt{1 + \left(\frac{u\tau}{h} \sin(kh)\right)^2}$$

With the varying speed case, the coefficient $\frac{u\tau}{h}$ was smaller during the whole run, since the maximum speed u attained will be 1.5 ft/min. as compared to 2 ft/min. in the fixed u case.

We see that the smaller the speed u the smaller the magnification (with everything else being fixed).

If we have run the simulation a little longer for the varying speed case, we will see the instability with explicit FTCS. This below is a diagram showing 2 runs using the explicit FTCS both with $u = \frac{t}{20} \text{ ft/min.}$ one was run for 30 minutes, and the second for 53 minutes. The run to 30 minutes showed no instability while the run for 53 minutes showed the instability. This shows the explicit FTCS will eventually become unstable.



This is an animation of the above

4.6 case 6

In this case, the time step is increased so that $\frac{u\tau}{h}$ is just above the CFL condition.

Notice now that the Explicit LAX method become unstable as expected. The other implicit methods remain stable. the explicit FTCS method now is completely unstable. The implicit FTCS method is starting to become less accurate.

$$\tau = 0.05025 \text{ sec}, h = 0.1 \text{ ft}, \frac{u\tau}{h} = \frac{2 \times 0.05025}{0.1} = 1.005 > 1$$

Speed	Method	CPU time (sec)	RMSE	Animation (2D)	plots
U=2	Explicit FTCS	0.7	blows up	N/A blows up	
	Explicit LAX	0.25	0.1006		
	Implicit FTCS	0.5	0.13945		
	C-R	0.468	0.01104		
U=t/20	Explicit FTCS	0.28	blows up	N/A blows up	
	Explicit LAX	0.31	0.04385		
	Implicit FTCS	0.45	0.0428		
	C-R	0.56	0.01317		

Notice that explicit LAX takes much less CPU than any other method.

4.7 case 7

$$\tau = 0.06 \text{ sec}, h = 0.1 \text{ ft}, \frac{u\tau}{h} = \frac{2 \times 0.06}{0.1} = 1.2 > 1$$

Speed	Method	CPU time (sec)	RMSE	Animation (2D)	plots
U=2	Explicit FTCS	0.65	blows up	N/A blows up	
	Explicit LAX	0.9	blows up		
	Implicit FTCS	0.42	0.1531		
	C-R	0.41	0.01244		
U=t/20	Explicit FTCS	0.265	blows up	N/A blows up	
	Explicit LAX	0.29	0.01389		
	Implicit FTCS	0.36	0.0493		
	C-R	0.36	0.01525		

Notice that the CPU for the implicit method when speed is fixed is now higher than the CPU for the explicit methods. This can be explained as follows: since the time step now is larger than before, the number of times to solve $Ax = b$ has been reduced. This made the implicit methods faster.

This implies that

Using a relatively large time step, implicit methods become faster than the explicit methods.

4.8 case 8

$$\tau = 0.07 \text{ sec}, h = 0.1 \text{ ft}, \frac{u\tau}{h} = \frac{2 \times 0.07}{0.1} = 1.4 > 1$$

Speed	Method	CPU time (sec)	RMSE	Animation (2D)	plots
U=2	Explicit FTCS	0.5	blows up	N/A blows up	
	Explicit LAX	0.89	blows up		
	Implicit FTCS	0.453	0.1653		
	C-R	0.36	0.01403		
U=t/20	Explicit FTCS	0.234	blows up	N/A blows up	
	Explicit LAX	0.2187	0.01564		
	Implicit FTCS	0.344	0.0557		
	C-R	0.312	0.0174		

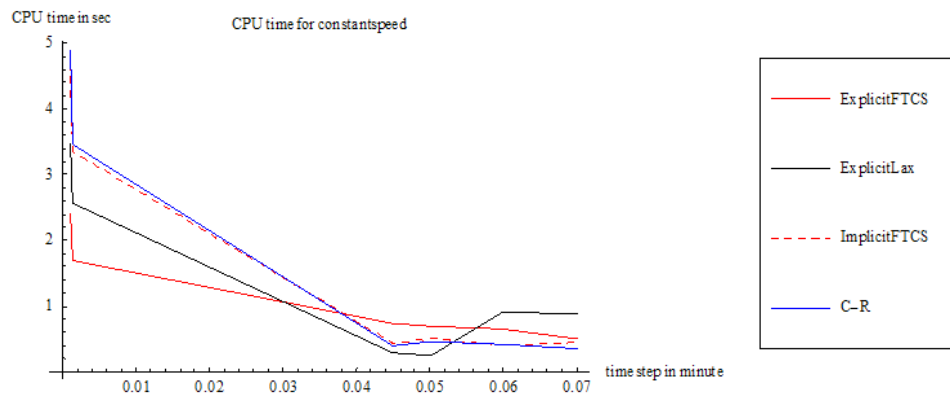
4.9 CPU comparison tables

As expected, CPU time usage will be less as the time step is increased. There is an anomaly noted where the CPU time increased for the Lax method when the time step is increased from 0.05025 to 0.06, This needs further investigation.

This table below summarizes the CPU time in seconds used by each method for the case of **constant speed** as time step is increased.

τ sec	<i>Explicit FTCS</i>	<i>Explicit LAX</i>	<i>Implicit FTCS</i>	<i>C - R</i>
0.0001	20	31	45	49
0.001	2.42	3.48	4.7	4.9
0.0013	1.9	2.78	3.7	3.9
0.0015	1.7	2.56	3.34	3.45
0.045	0.73	0.281	0.43	0.4
0.05025	0.7	0.25	0.5	0.468
0.06	0.65	0.9	0.4	0.41
0.07	0.5	0.89	0.45	0.36

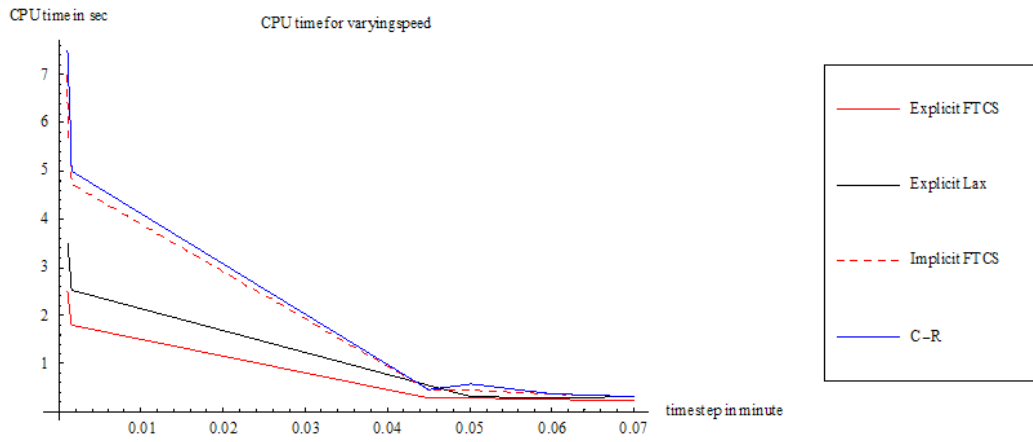
This is the plot of the above table



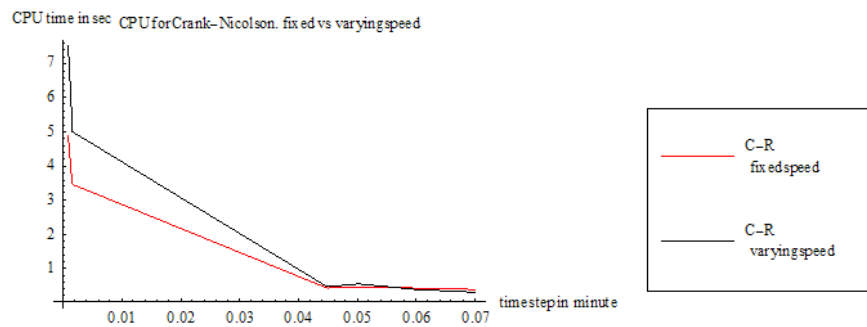
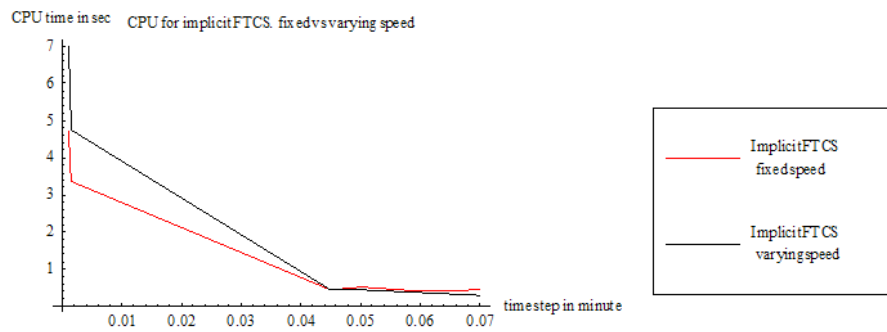
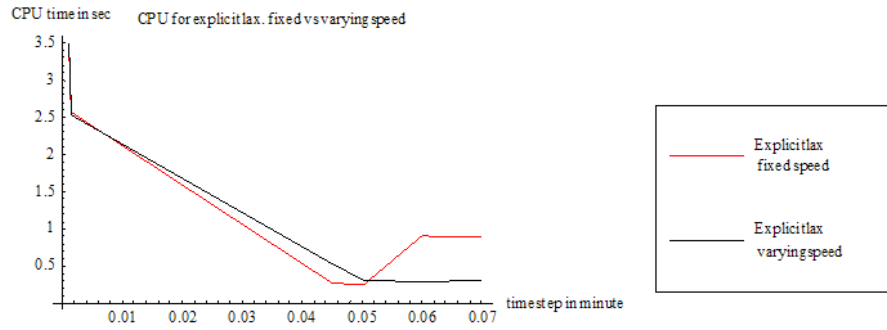
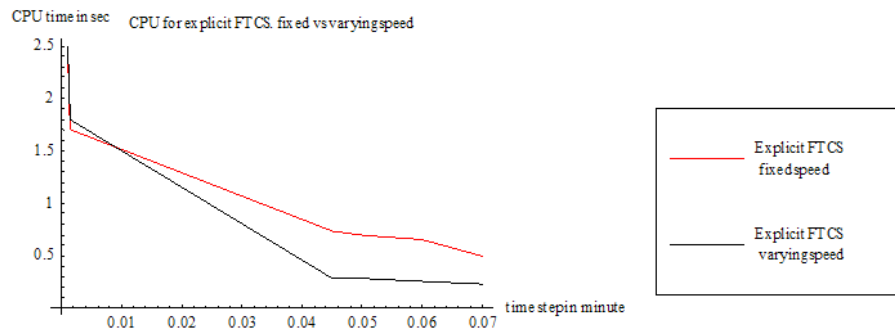
This table below summarizes the CPU time in seconds used by each method for the case of **varying speed** as time step is increased.

τ sec	<i>Explicit FTCS</i>	<i>Explicit LAX</i>	<i>Implicit FTCS</i>	<i>C - R</i>
0.0001	21	31	67	69
0.001	2.5	3.5	7	7.5
0.0013	2	2.9	5.56	6
0.0015	1.8	2.53	4.73	5
0.045	0.28	0.54	0.45	0.45
0.05025	0.28	0.31	0.45	0.56
0.06	0.265	0.29	0.36	0.36
0.07	0.23	0.22	0.33	0.31

This is the plot of the above table



This plot below compares the CPU time for each method when the speed is constant vs. when the speed was changing with time.



4.10 Accuracy comparison tables

This table below summarizes the RMS error from each numerical method as a function of changing the time step size. This is for case of **constant speed**.

<i>time step</i>	<i>Explicit FTCS</i>	<i>Explicit LAX</i>	<i>Implicit FTCS</i>	<i>C – R</i>
0.0001	0.0546	0.0543	0.0548	0.0544
0.001	0.01264	0.0057	0.00742	0.00575
0.0013	0.0494	0.01125	0.01245	0.00128
0.0015	0.15249	0.00056	0.009	0.0056
0.045	<i>blows up</i>	0.000162	0.1306	0.01028
0.05025	<i>blows up</i>	0.1006	0.1394	0.011
0.06	<i>blows up</i>	<i>blows up</i>	0.1531	0.01244
0.07	<i>blows up</i>	<i>blows up</i>	0.1653	0.01403

Notice that the Lax method became more accurate when the time step was increased from 0.0001 to 0.04 seconds, then it starts to become less accurate as time step is increased. This is counter intuitive to what one can expect. It will be interesting to investigate this further to obtain a mathematical explanation for this strange phenomena.

The accuracy of the implicit FTCS, and C-R also increased slightly as the time step became larger from 0.0001 to 0.0015, then the implicit FTCS became worst in terms of accuracy as the time step increased.

C-R method accuracy did not deteriorate as much with increasing the time step. This shows the C-R scheme to be more robust.

This table below summarizes the RMS error from each numerical method as a function of changing the time step size. This is for case of **changing speed**.

<i>time step</i>	<i>Explicit FTCS</i>	<i>Explicit LAX</i>	<i>Implicit FTCS</i>	<i>C – R</i>
0.0001	0.003	0.003	0.003	0.0030
0.001	0.00352	0.00329	0.0033	0.0033
0.0013	0.00365	0.00331	0.00346	0.0033
0.0015	0.0038	0.00336	0.0035	0.00337
0.045	<i>blows up</i>	0.01117	0.0386	0.0119
0.05025	<i>blows up</i>	0.04385	0.0428	0.01317
0.06	<i>blows up</i>	0.01389	0.0493	0.01525
0.07	<i>blows up</i>	0.01564	0.0557	0.0174

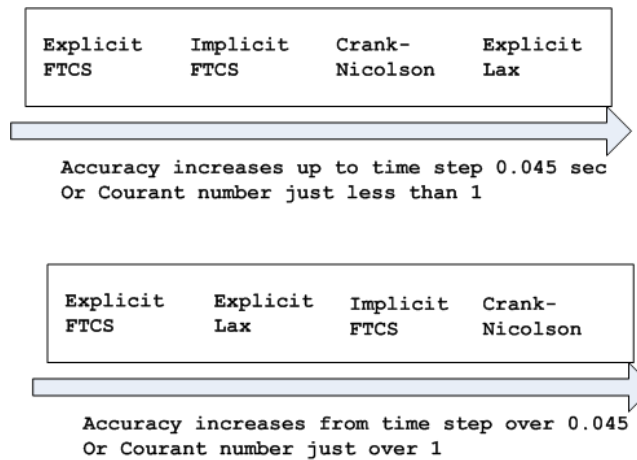
The effect of having the speed defined as $\mu = \frac{t}{20}$ is to delay instability for the explicit methods as time step is increased. Notice also here the case where the Lax method became more accurate as the time step is increased from 0.0001 to 0.0015.

5 Conclusion

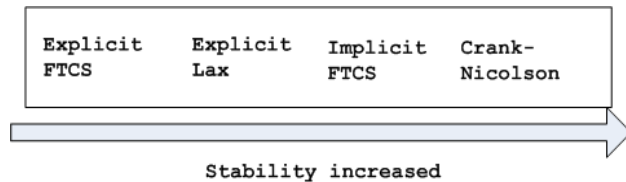
4 different numerical finite difference schemes are examined for CPU time, stability and accuracy in solving the advection PDE for constant speed and for a speed which is a function of time.

For accuracy, an interesting result is observed. The Lax scheme is the most accurate for Courant number close to unity. This means as the time step is *increased*, the Lax become more accurate of the 4 methods. But beyond the CFL condition, Both explicit methods (FTCS and Lax) became less accurate. Explicit FTCS became unstable sooner than Lax, while the implicit methods remained stable.

The implicit FTCS was less accurate than the C-R method. This implies that one should use the Lax method if one can be satisfied with a time step such that the courant number is close to a unit.



For stability, Crank-Nicolson was the most stable of all methods. Stability by itself is not sufficient condition to use to select a numerical scheme. It must also be accurate. The C-R method has both these properties for the range of the time steps considered. But as mentioned above, there is a range of time steps in which the Lax method is more accurate than all the other methods.



For CPU usage, the explicit methods used less CPU time when the time step was small, up to 0.0015 sec. This can be explained as follows: for small step size, the number of time to solve $Ax = b$ is large. Hence the implicit methods will be slower. As the time step is increased to the range of 0.045sec and over, the implicit methods actually became more CPU efficient due to the fact that the number of times to solve $Ax = b$ is less because the number of steps is less.

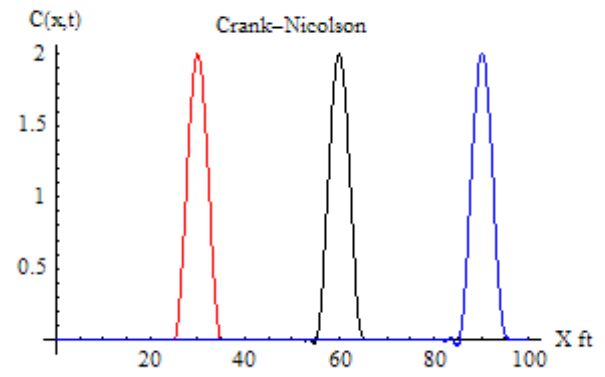
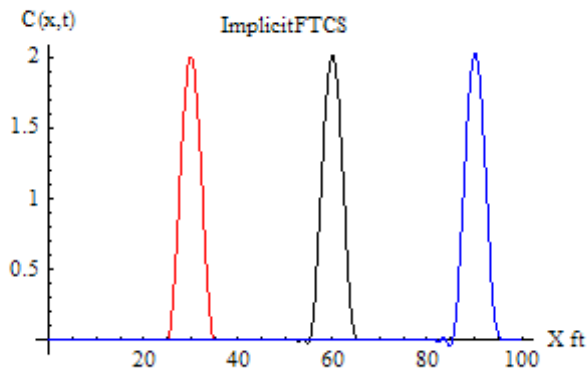
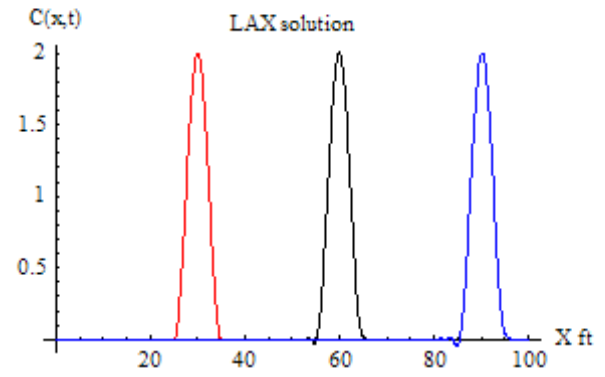
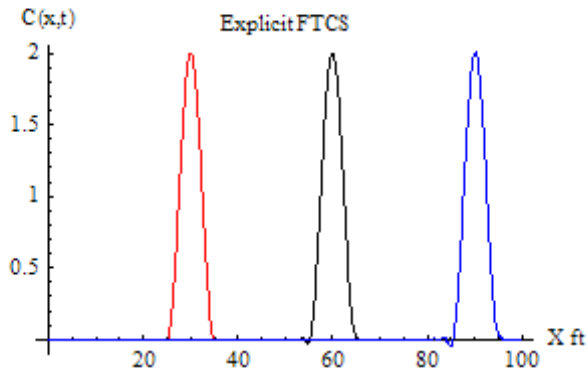
In conclusion, the selection of a finite difference scheme depends on many factors. Stability and accuracy being the most important. The time step size plays a critical rule. For Courant number close to a unity, the Lax method is the most attractive. For larger time steps, the C-R method should be considered.

6 Appendix

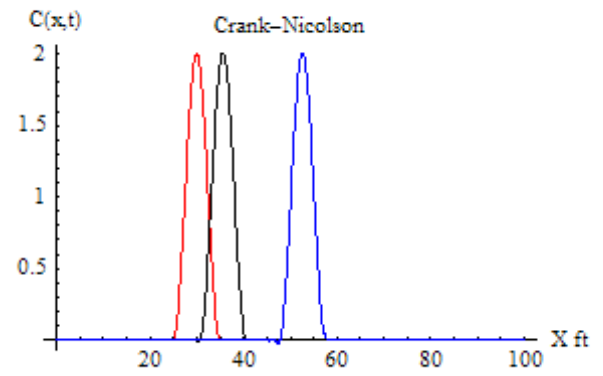
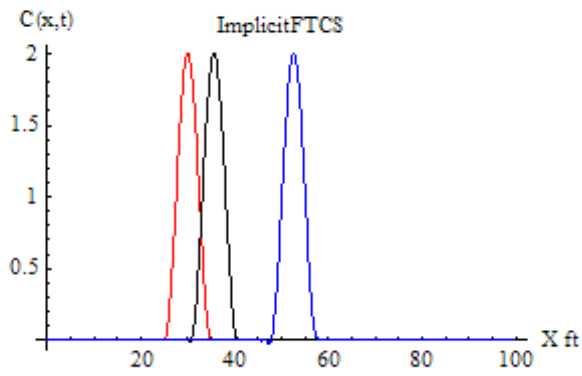
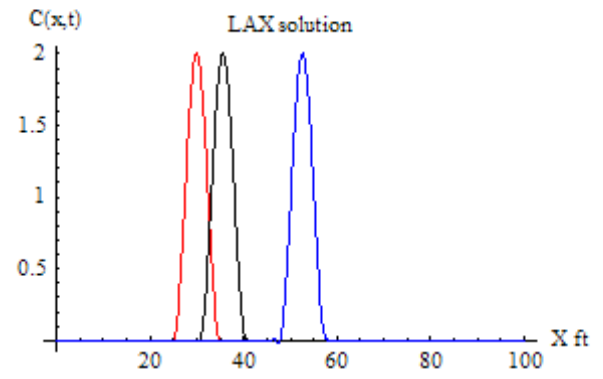
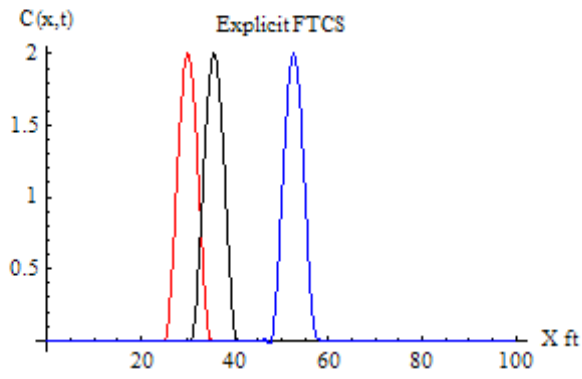
6.1 Plots

6.1.1 case 1

Solution at $t=0,15,30$ minutes.
speed $U=2$ ft/min, $dt=0.0001$ min. $dx=0.1$ ft.

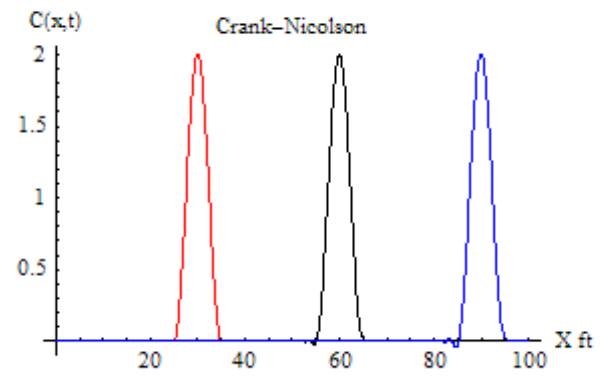
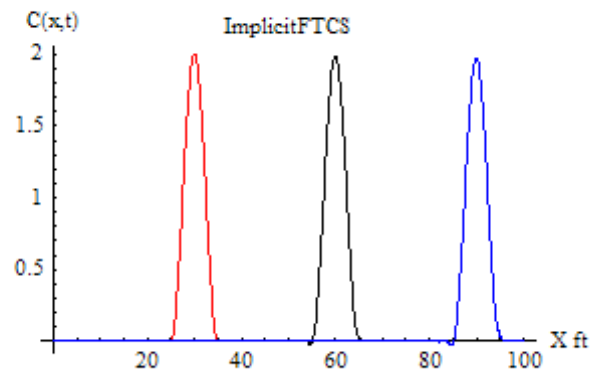
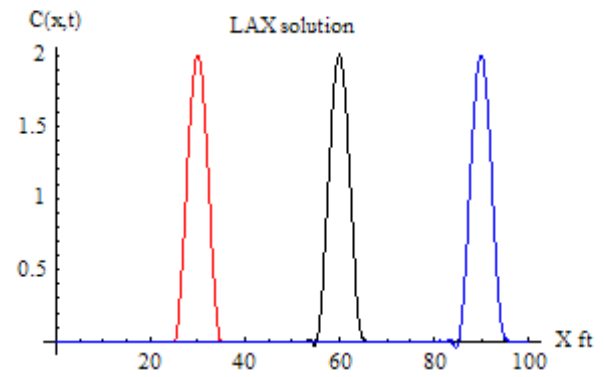
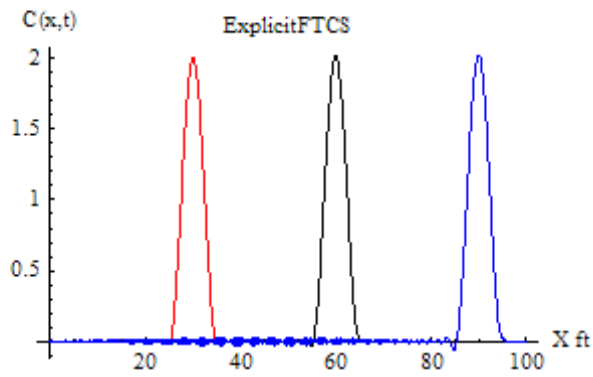


Solution at $t=0, 15, 30$ minutes.
speed $U=t/20$ ft/min, $dt=0.0001$ min. $dx=0.1$ ft.

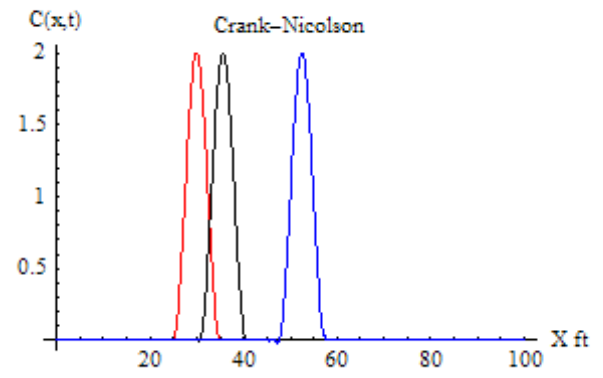
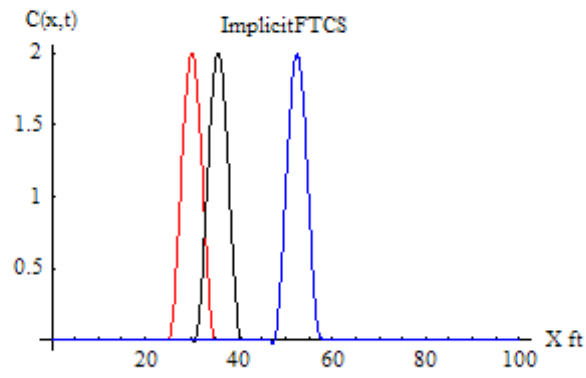
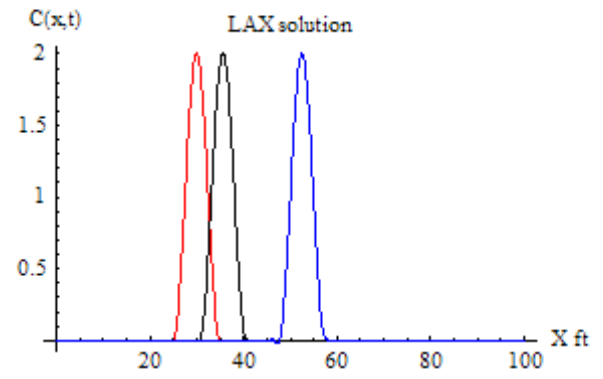
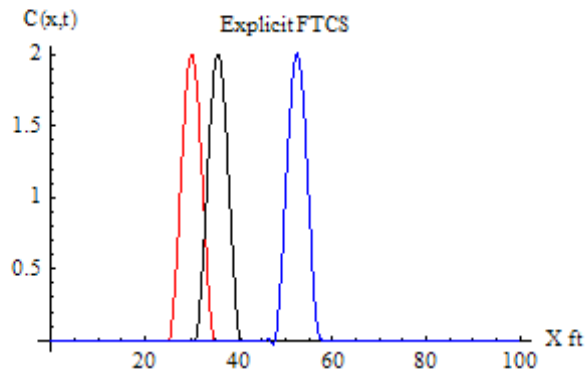


6.1.2 case 2

Solution at $t=0,15,30$ minutes.
speed $U=2$ ft/min, $dt=0.001$ min. $dx=0.1$ ft.

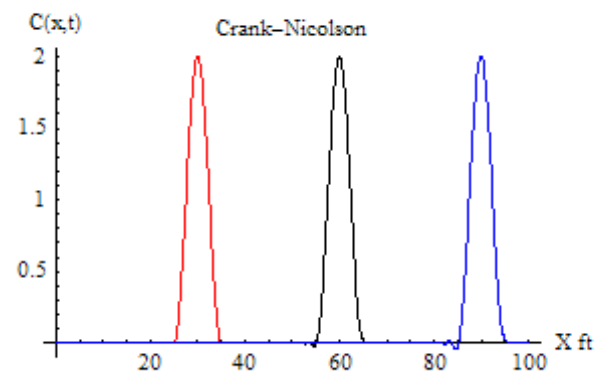
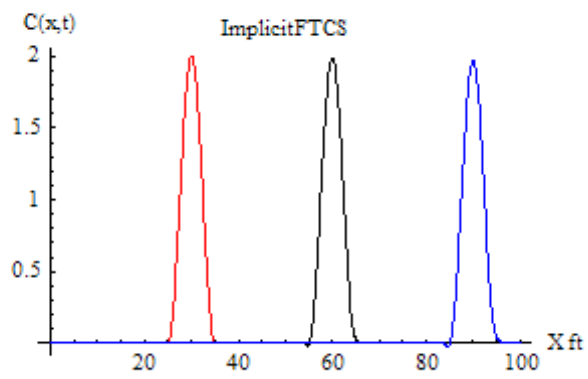
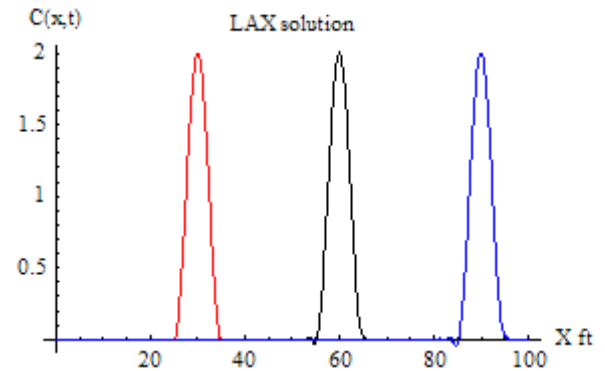
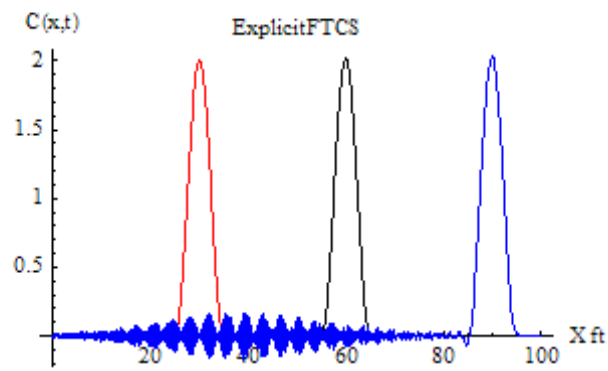


Solution at $t=0,15,30$ minutes.
speed $U=t/20$ ft/min, $dt=0.001$ min. $dx=0.1$ ft.

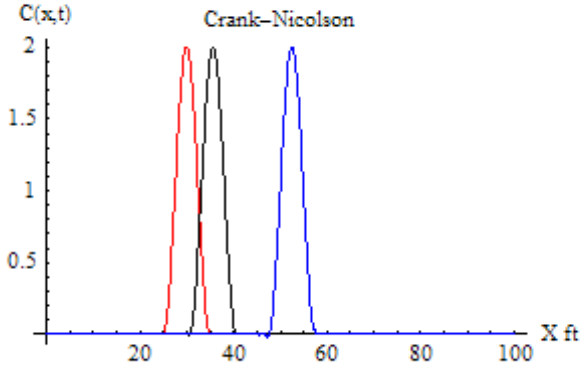
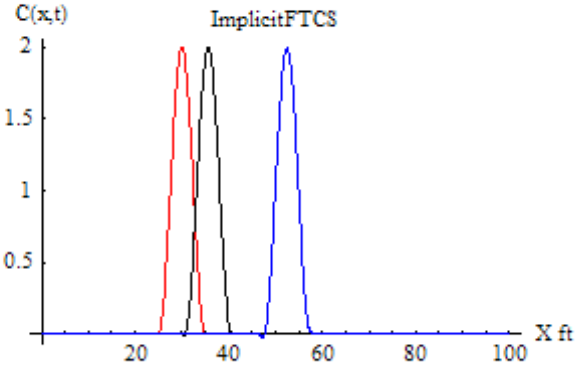
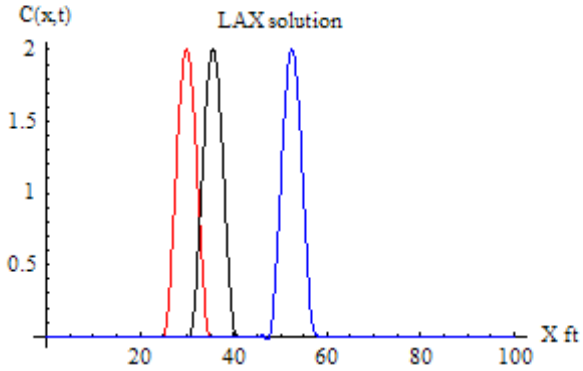
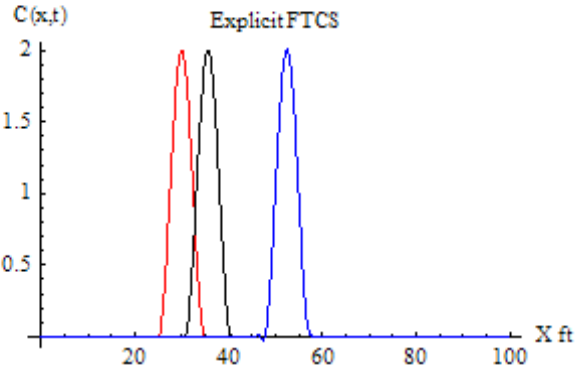


6.1.3 case 3

Solution at $t=0,15,30$ minutes.
speed $U=2$ ft/min, $dt=0.0013$ min. $dx=0.1$ ft.

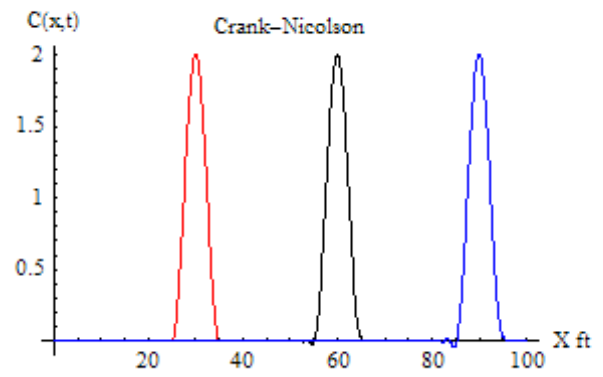
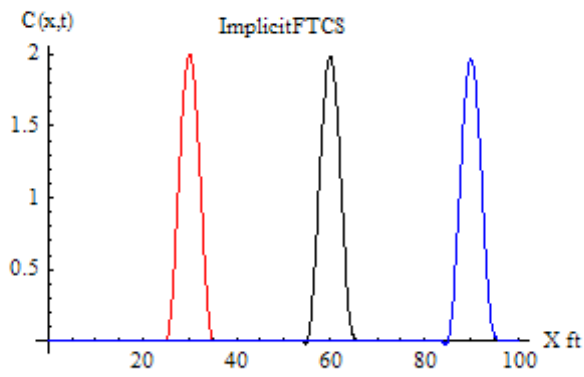
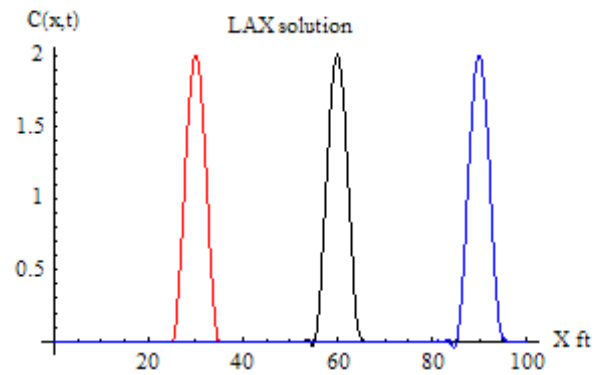
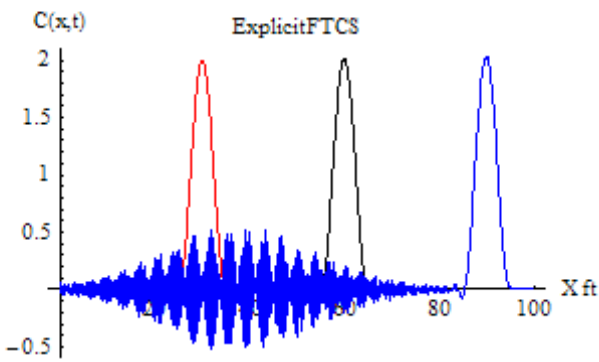


Solution at $t=0, 15, 30$ minutes.
speed $U=t/20$ ft/min, $dt=0.0013$ min. $dx=0.1$ ft.

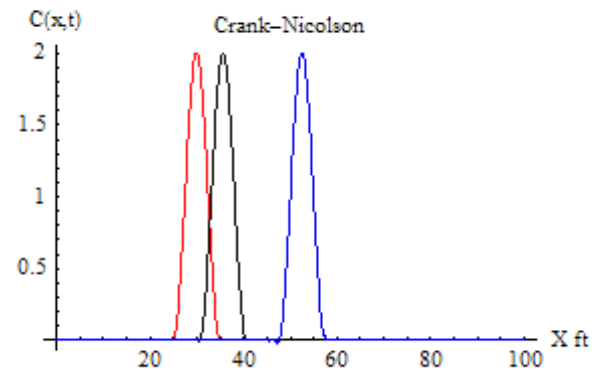
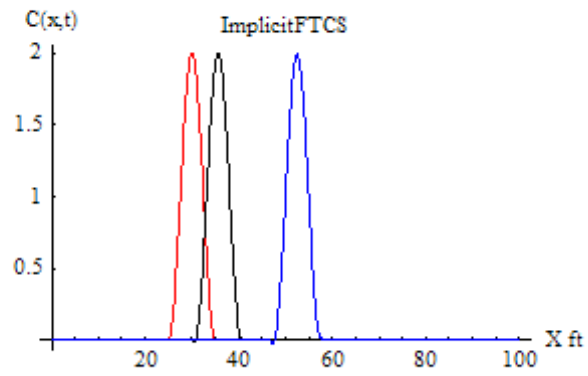
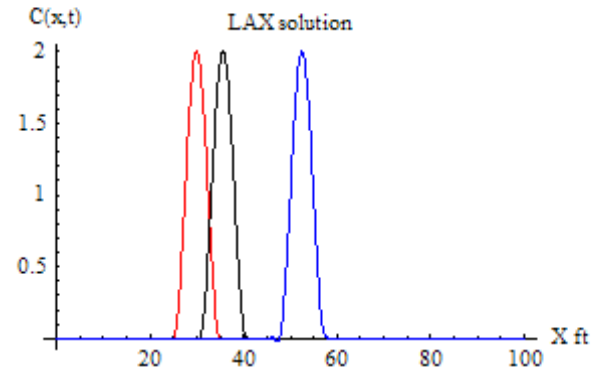
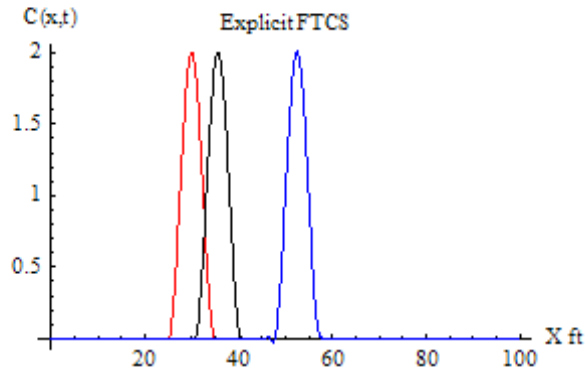


6.1.4 case 4

Solution at $t=0,15,30$ minutes.
speed $U=2$ ft/min, $dt=0.0015$ min. $dx=0.1$ ft.

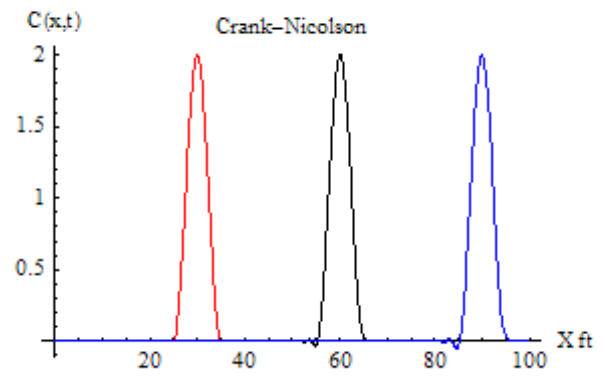
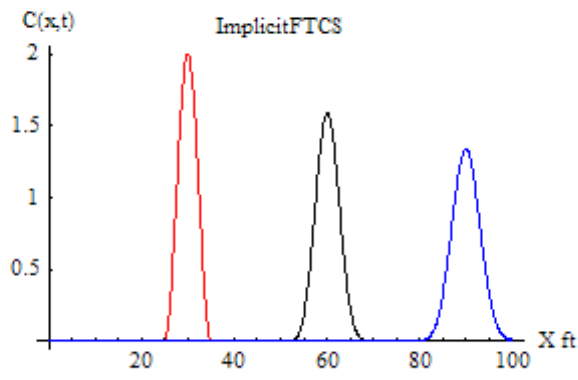
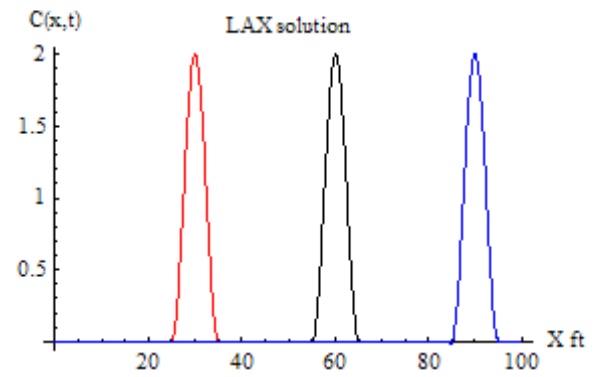
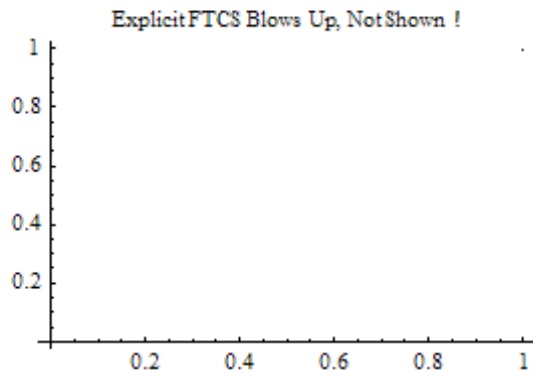


Solution at $t=0, 15, 30$ minutes.
speed $U=t/20$ ft/min, $dt=0.0015$ min. $dx=0.1$ ft.

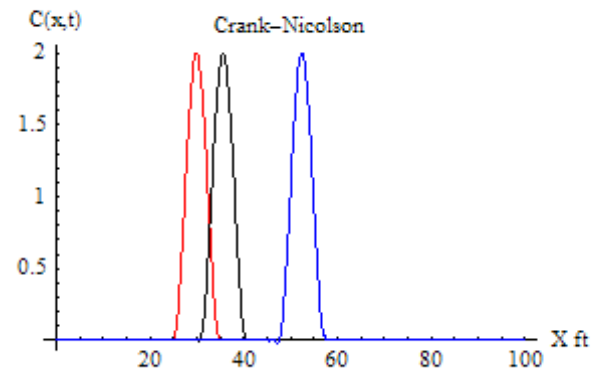
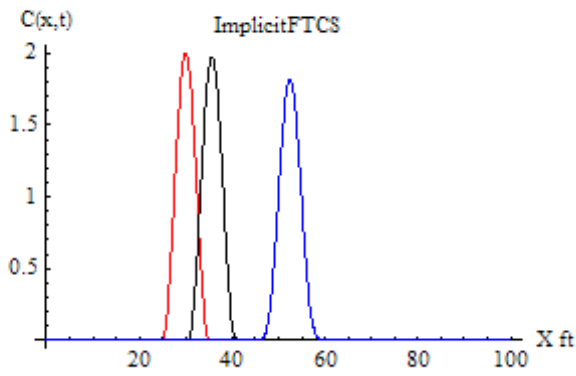
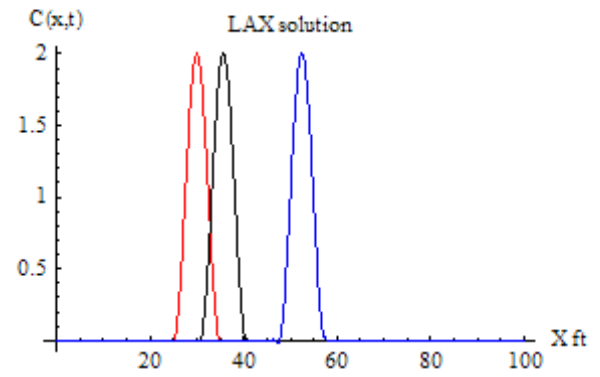
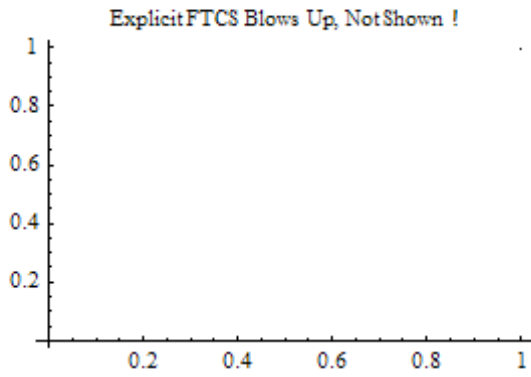


6.1.5 case 5

Solution at $t=0,15,30$ minutes.
speed $U=2$ ft/min, $dt=0.045$ min. $dx=0.1$ ft.

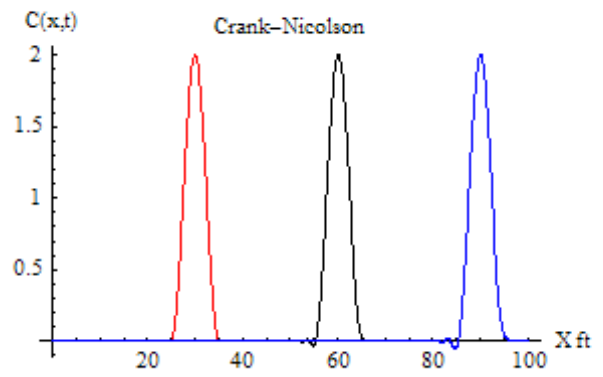
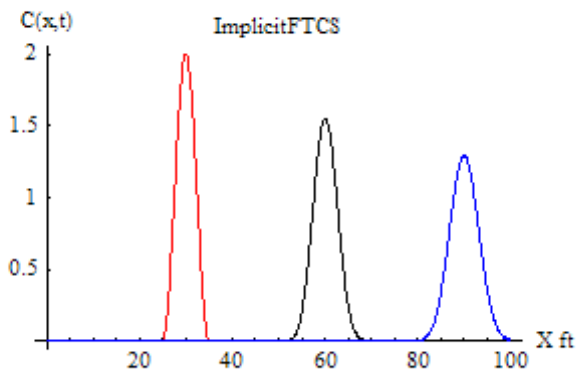
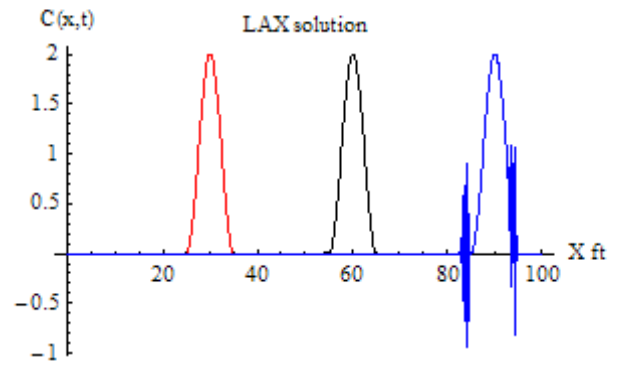
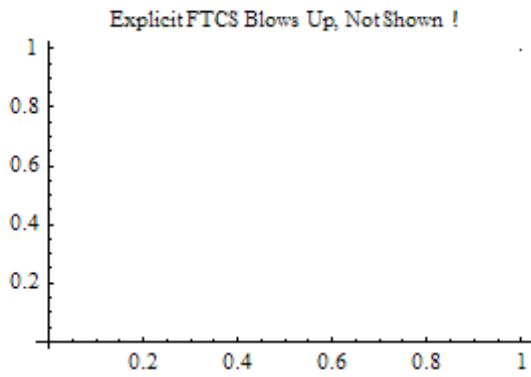


Solution at $t=0,15,30$ minutes.
speed $U=t/20$ ft/min, $dt=0.045$ min. $dx=0.1$ ft.

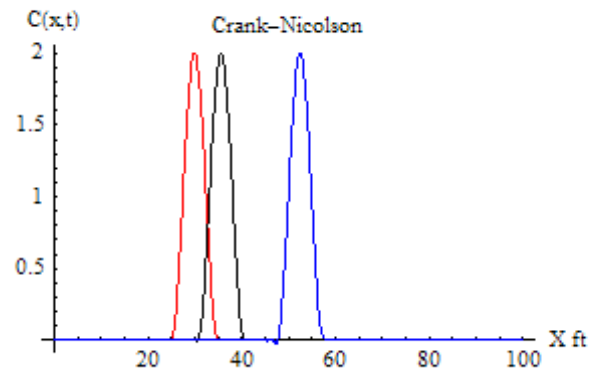
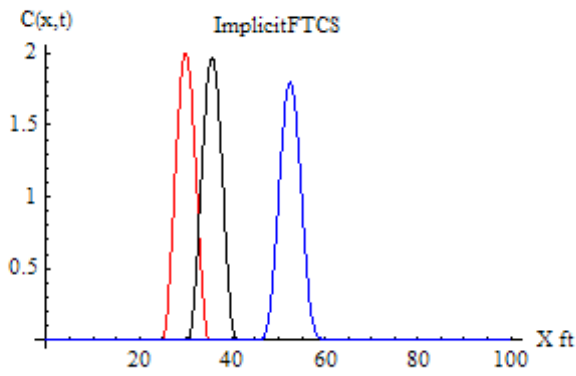
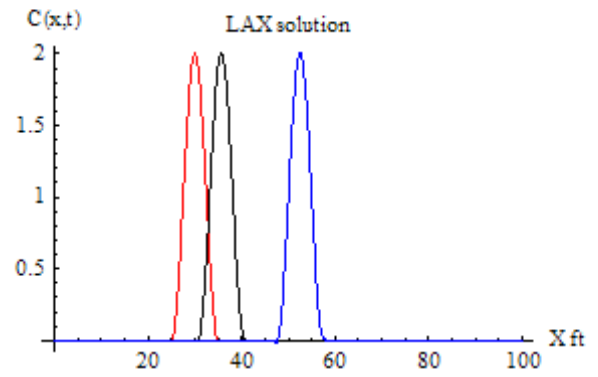
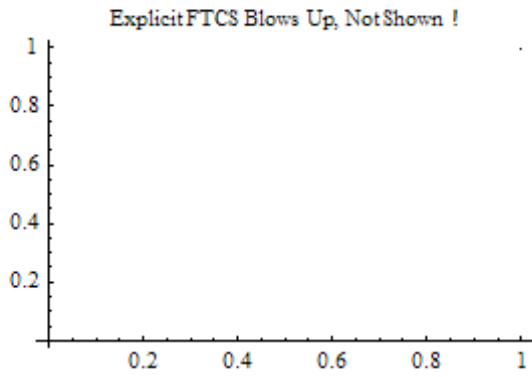


6.1.6 case 6

Solution at $t=0,15,30$ minutes
speed $U=2$ ft/min, $dt=0.05025$ min. $dx=0.1$ ft.

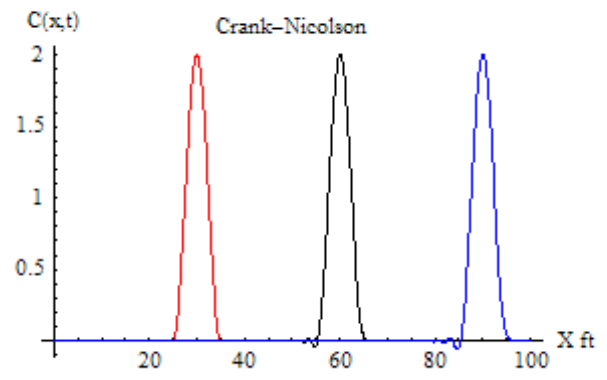
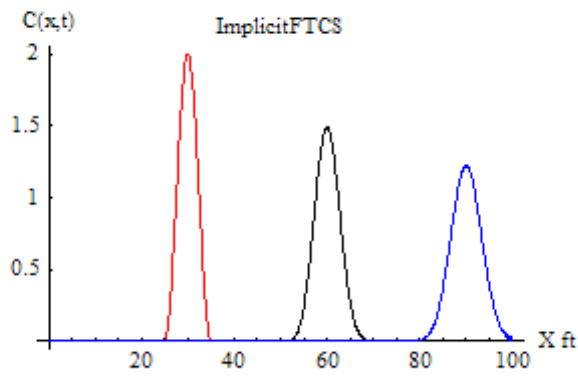
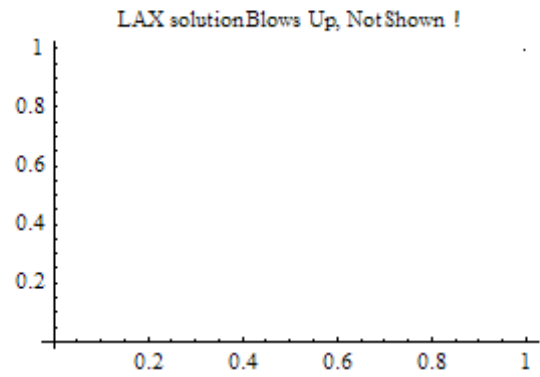
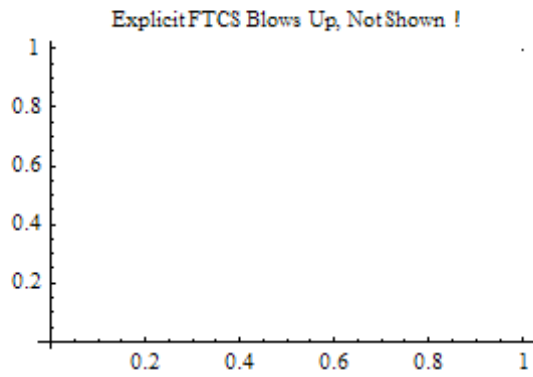


Solution at $t=0, 15, 30$ minutes
speed $U=t/20$ ft/min, $dt=0.05025$ min. $dx=0.1$ ft.

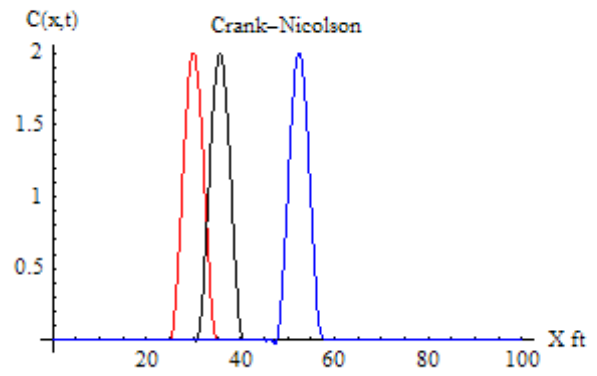
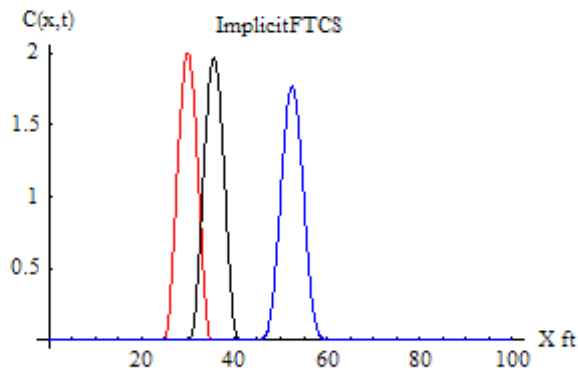
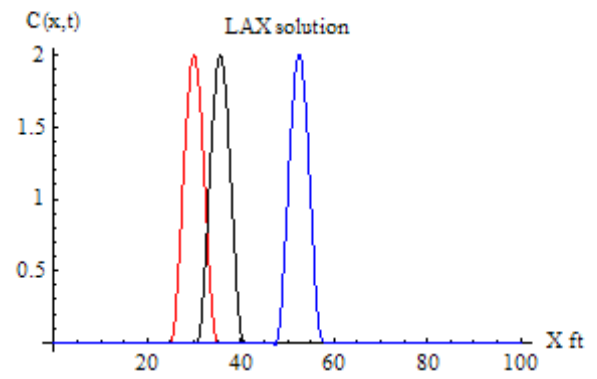
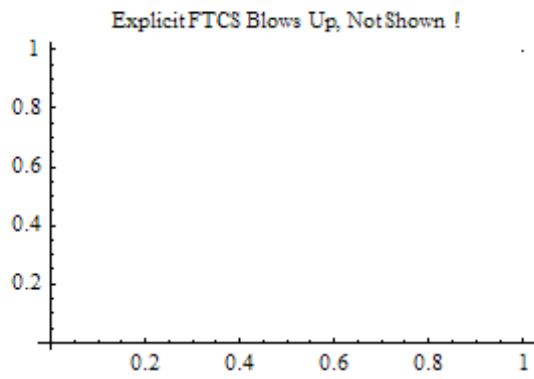


6.1.7 case 7

Solution at t=0,15,30 minutes.
speed $U=2$ ft/min, $dt=0.06$ min. $dx=0.1$ ft

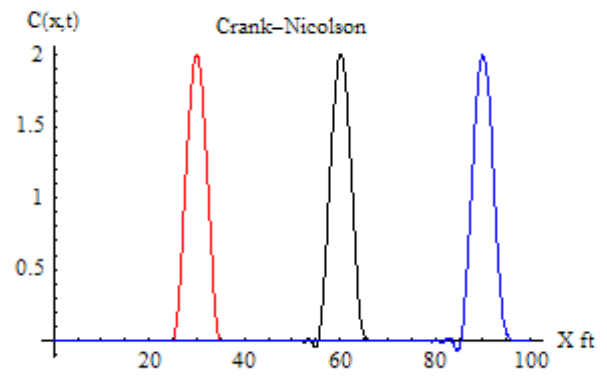
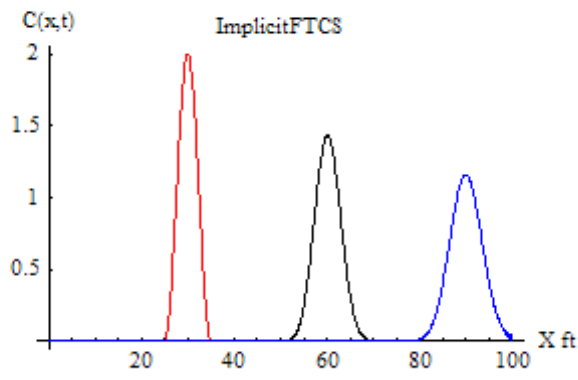
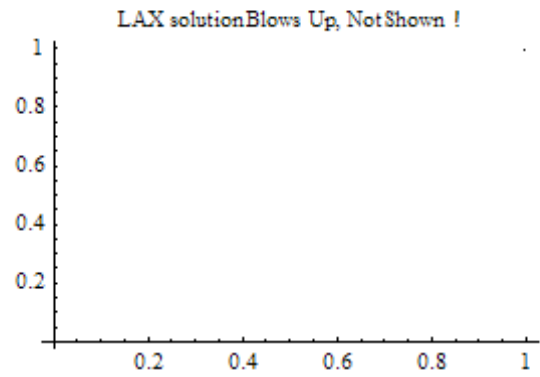
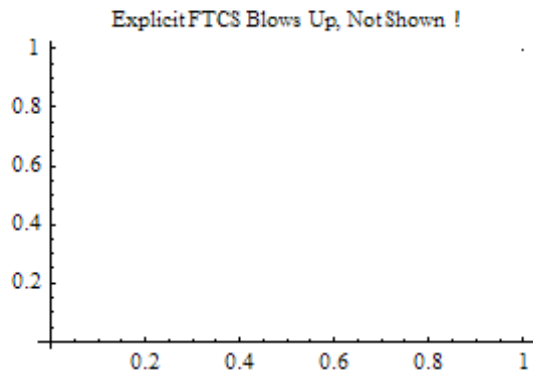


Solution at $t=0, 15, 30$ minutes
speed $U=t/20$ ft/min, $dt=0.06$ min. $dx=0.1$ ft

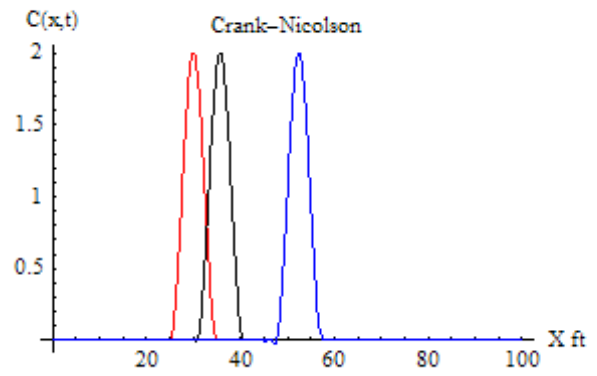
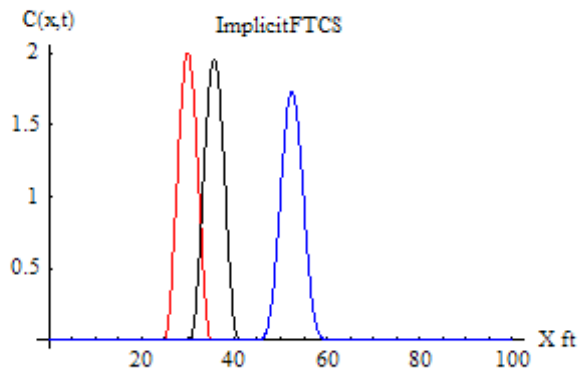
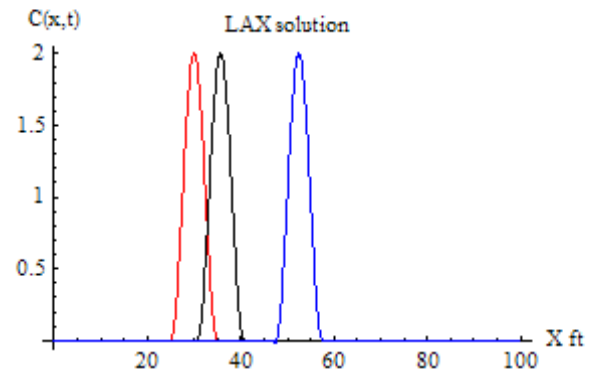
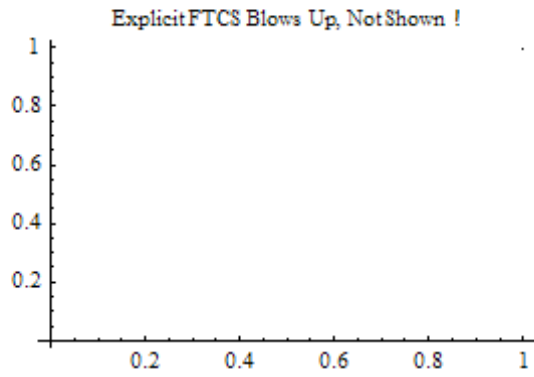


6.1.8 case 8

Solution at t=0,15,30 minutes.
speed $U=2$ ft/min, $dt=0.07$ min. $dx=0.1$ ft



Solution at $t=0, 15, 30$ minutes
speed $U=t/20$ ft/min, $dt=0.07$ min. $dx=0.1$ ft



6.2 Source code

```
1  !*****
2  !*
3  !* Solve the advection PDE using Explicit FTCS,
4  !* Explicit Lax, Implicit FTCS, and implicit Crank-Nicolson
5  !* methods for constant and varying speed.
6  !*
7  !* Solve  $dc/dt = -u dc/dx$ 
8  !*  $u = t/20$  ft/minute
9  !* and
10 !* u constant
11 !*
12 !* Compiler used: gnu 95 (g95) on Cygwin. Gcc 3.4.4
13 !* Date: June 20 2006
14 !*
15 !* by Nasser Abbasi
16 !*****
17
18 PROGRAM advection
19   IMPLICIT NONE
20
21   REAL      :: DT,DX,max_run_time,length,snapshot_Δ, &
22             first_limit,second_limit
23   INTEGER   :: N,SNAPSHOTS
24   character(10) :: cmd_arg ! to read time step from command line
25
26   INTEGER :: method ! 1=FTCS, 2=LAX, 3=Implicit FTCS, 4=C-R
27   INTEGER :: mode   ! 1=Fixed wind speed, 2=speed function of time
28
29   REAL      :: t_start, t_end, cpu_time_used,end_line(1002)
30   INTEGER   :: ALL_DATA_FILE_ID
31   PARAMETER(ALL_DATA_FILE_ID=900)
32
33   ! Initialize data. All methods will use the same
34   ! parameters to make comparing them easier
35
36   ! read  $\Delta t$  from command line.
37   CALL getarg(1,cmd_arg)
38   cmd_arg=TRIM(cmd_arg)
39   print *,'= ', cmd_arg
40   read(cmd_arg,*)dt    ! $\Delta$  in time, in minutes
41
42   print *,'Dt=',DT
43
44   N      = 1000      ! number of grid points in space
45   length = 100      ! length of space solution in feet
46
47   first_limit = 0.25*length
48   second_limit = 0.35*length
49
50   DX = length/N      !  $\Delta$  in space, in feets
51
52   max_run_time = 30.0 ! how long to run for in minutes
53   SNAPSHOTS    = 200  ! number of snapshots per run. Used for animation
54
55   snapshot_Δ = max_run_time / SNAPSHOTS ! time between each snap shot
56
57   print *,'DT=',DT,' minutes, DX=',DX,' feets'
58   print *,'taking snapshots every ', snapshot_Δ , ' minutes'
59
60   DO mode=1,2
61     print*,'=====> processing mode ',mode
62     DO method=1,4 ! No enumeration data types in Fortran 90
63
64       CALL CPU_TIME(t_start) ! get current CPU time
65       CALL process(mode,method,N,DT,DX,max_run_time,snapshot_Δ,&
66                 first_limit,second_limit)
67       CALL CPU_TIME(t_end) ! get current CPU time
68
69       cpu_time_used = t_end - t_start
70
71       WRITE(*,FMT='(A,I2,A,F12.5)') 'CPU TIME used for method', method, ' = ', cpu_time_used
72       ! Now record test case parameters in last line
```

```

73     end_line=0
74     end_line(1)=cpu_time_used
75     end_line(2)=DT
76     end_line(3)=DX
77     end_line(4)=mode
78     end_line(5)=method
79
80     WRITE(UNIT=ALL_DATA_FILE_ID,FMT=*) end_line
81     CLOSE(ALL_DATA_FILE_ID)
82
83     END DO
84 END DO
85
86 END PROGRAM advection
87 !*****
88 !*
89 !*
90 !*****
91 SUBROUTINE process(mode,method,N,DT,DX,max_run_time,snapshot_Δ,&
92                first_limit,second_limit)
93     IMPLICIT NONE
94
95     INTEGER, INTENT(IN) :: mode,method,N
96     REAL,    INTENT(IN) :: DT,DX,max_run_time,snapshot_Δ,&
97                first_limit,second_limit
98
99     INTEGER :: I
100    LOGICAL :: snap_shot_at_15_taken
101    INTEGER :: ALL_DATA_FILE_ID
102    PARAMETER(ALL_DATA_FILE_ID=900)
103    REAL    :: snap_current_time
104    REAL    :: current_time
105    REAL    :: C(N)      ! current solution
106    REAL    :: CNEW(N)   ! future solution
107    REAL    :: CEXACT(N) ! current exact solution
108    REAL    :: current_first_limit
109    REAL    :: A(N,N),aa(N),b(2:N),cc(N-1),CTEMP(N) ! for C-R and implicit FTCS
110    REAL    :: K,speed
111    REAL    :: error,RMS ! root mean square error between current and initial sol.
112
113    current_time      = 0.
114    snap_current_time = 0.
115
116    CALL initialize_solution(C,N,DX,first_limit,second_limit)
117    CEXACT = C
118    current_first_limit = first_limit
119
120    CALL pre_loop_initialization(mode,method,current_time,K, &
121                                DT,DX,N,C,ALL_DATA_FILE_ID, &
122                                A,aa,b,cc )
123
124    snap_shot_at_15_taken=.FALSE.
125
126    DO WHILE(current_time < max_run_time)
127
128        IF( snap_current_time ≥ snapshot_Δ ) THEN
129            snap_current_time = 0.
130            WRITE( UNIT=ALL_DATA_FILE_ID, FMT=*) current_time, error, C
131        END IF
132
133        SELECT CASE(method)
134
135        CASE( 1:2 )
136
137            IF(method==1) THEN ! ftcs
138                IF(mode==2) THEN
139                    K = speed(mode,current_time)*DT/(2.*DX)
140                ENDIF
141
142                DO I = 2,N-1
143                    CNEW(I) = C(I) - K * ( C(I+1) - C(I-1) )
144                END DO
145            ELSE !lax
146                IF(mode == 2) THEN
147                    K = speed(mode,current_time)*DT/(DX)
148                ENDIF

```

```

149
150     DO I = 2,N-1
151         CNEW(I) = C(I) - K/2. * ( C(I+1) - C(I-1) ) + &
152             (K**2.)/2 * ( C(I+1) +C(I-1)-2.*C(I) )
153     END DO
154 END IF
155
156 CNEW(1) = C(1)
157 CNEW(N) = C(N) ! Boundary conditions
158 C=CNEW
159
160 CASE( 3 ) ! implicit ftcs
161
162 IF( mode == 2 ) THEN ! only need to update Matrix for varying U
163     K = speed(mode,current_time)*DT/(2.*DX)
164
165     CALL init_A_matrix(A,K,N)
166     CALL init_diagonal_vectors(N,A,cc,aa,b)
167 END IF
168
169 CALL solve_thomas_algorithm(N,aa,b,cc,C,CNEW)
170 C = CNEW
171
172 CASE( 4 ) ! C-R
173
174 IF(mode == 2) THEN !only need to update A if U changes
175     K = speed(mode,current_time)*DT/(4*DX) ! C-R
176     CALL init_A_matrix(A,K,N)
177     CALL init_diagonal_vectors(N,A,cc,aa,b)
178 END IF
179
180 CTEMP(1) = C(1)
181 CTEMP(N) = C(N)
182
183 DO I=2,N-1
184     CTEMP(I)=C(I)+K*C(I-1)-K*C(I+1)
185 END DO
186
187 CALL solve_thomas_algorithm(N,aa,b,cc,CTEMP,C)
188
189 END SELECT
190
191 IF( current_time>=15.0 .AND. (.NOT. snap_shot_at_15_taken) ) THEN
192     snap_shot_at_15_taken = .TRUE.
193     CALL take_one_snap_shot(mode,method,15,N,C,DX)
194 END IF
195
196 current_time = current_time + DT
197 current_first_limit = current_first_limit + speed(mode,current_time)*DT
198 CALL get_current_exact_solution(CEXACT,N,current_first_limit,DX)
199 error = RMS(CEXACT,C,N)
200
201 snap_current_time = snap_current_time + DT
202
203 END DO
204
205 CALL take_one_snap_shot(mode,method,30,N,C,DX)
206
207 END SUBROUTINE process
208 !*****
209 !*
210 !*
211 !*****
212 SUBROUTINE pre_loop_initialization(mode,method,current_time,K,&
213     DT,DX,N,C,ALL_DATA_FILE_ID,&
214     A,aa,b,cc)
215 IMPLICIT NONE
216
217 INTEGER, INTENT(IN) :: mode,method,N,ALL_DATA_FILE_ID
218 REAL, INTENT(IN) :: C(N),DT,DX,current_time
219 REAL, INTENT(OUT) :: K,A(N,N),aa(N),b(2:N),cc(N-1)
220 REAL :: speed
221
222 SELECT CASE(method)
223 CASE( 1 ) ! FTCS
224

```

```

225     K = speed(mode,current_time)*DT/(2.*DX)
226
227     IF(mode==1) THEN
228         OPEN(UNIT=ALL_DATA_FILE_ID, file='expAll.txt') ! all time shots
229         CALL print_to_file(C,'exp0.txt',N,DX)
230     ELSE
231         OPEN(UNIT=ALL_DATA_FILE_ID, file='exp_extraAll.txt') ! all time shots
232         CALL print_to_file(C,'exp_extra0.txt',N,DX)
233     END IF
234
235 CASE( 2 )      ! Lax
236
237     K = speed(mode,current_time)*DT/(DX)
238
239     IF(mode==1) THEN
240         OPEN(UNIT=ALL_DATA_FILE_ID, file='laxAll.txt') ! all time shots
241         CALL print_to_file(C,'lax0.txt',N,DX)
242     ELSE
243         OPEN(UNIT=ALL_DATA_FILE_ID, file='lax_extraAll.txt') ! all time shots
244         CALL print_to_file(C,'lax_extra0.txt',N,DX)
245     END IF
246
247 CASE( 3 )      ! Implicit FTCS
248
249     K = speed(mode,current_time)*DT/(2.*DX)
250
251     CALL init_A_matrix(A,K,N)
252     CALL init_diagonal_vectors(N,A,cc,aa,b)
253
254     IF(mode==1) THEN
255         OPEN(UNIT=ALL_DATA_FILE_ID, file='impAll.txt') ! all time shots
256         CALL print_to_file(C,'imp0.txt',N,DX)
257     ELSE
258         OPEN(UNIT=ALL_DATA_FILE_ID, file='imp_extraAll.txt') ! all time shots
259         CALL print_to_file(C,'imp_extra0.txt',N,DX)
260     END IF
261
262 CASE( 4 )      ! C-R
263
264     K = speed(mode,current_time)*DT/(4*DX)      ! C-R
265
266     CALL init_A_matrix(A,K,N)
267     CALL init_diagonal_vectors(N,A,cc,aa,b)
268
269     IF(mode==1) THEN
270         OPEN(UNIT=ALL_DATA_FILE_ID, file='crAll.txt') ! all time shots
271         CALL print_to_file(C,'cr0.txt',N,DX)
272     ELSE
273         OPEN(UNIT=ALL_DATA_FILE_ID, file='cr_extraAll.txt') ! all time shots
274         CALL print_to_file(C,'cr_extra0.txt',N,DX)
275     END IF
276 END SELECT
277
278 WRITE( UNIT=ALL_DATA_FILE_ID, FMT=*) current_time,0, C
279
280 END SUBROUTINE pre_loop_initialization
281 !*****
282 !*
283 !*
284 !*****
285 SUBROUTINE init_diagonal_vectors(N,A,cc,aa,b)
286     IMPLICIT NONE
287
288     INTEGER, INTENT(IN) ::N
289     REAL, INTENT(IN)    ::A(N,N)
290     REAL, INTENT(OUT)  ::aa(N),b(2:N),cc(N-1)
291
292     INTEGER ::I,J
293
294     J=2
295     DO I=1,N-1
296         cc(I)=A(I,J)
297         J=J+1
298     END DO
299     cc(1)=0
300

```

```

301 DO I=1,N
302   aa(I)=A(I,I)
303 END DO
304
305 J=1
306 DO I=2,N
307   b(I)=A(I,J)
308   J=J+1
309 END DO
310
311 END SUBROUTINE init_diagonal_vectors
312 !*****
313 !*
314 !*
315 !*****
316 SUBROUTINE initialize_solution(C,N,DX,first_limit,second_limit)
317   IMPLICIT NONE
318
319   INTEGER, INTENT(IN)      :: N
320   REAL, INTENT(IN)        :: DX,first_limit,second_limit
321   REAL, INTENT(INOUT)    :: C(0:N-1)
322
323   INTEGER :: I
324   REAL    :: x, PI,av,R
325
326   PARAMETER( PI = ACOS(-1.) )
327
328   x = 0
329   av = (second_limit+first_limit)/2.0
330   R = av - first_limit
331
332   C = 0.0
333
334   DO I=0,N-1
335
336     IF( x ≥ first_limit .AND. x ≤ second_limit ) THEN
337       C(I) = 1 + COS( PI * (x-av)/R )
338     END IF
339
340     x = x + DX
341   END DO
342
343 END SUBROUTINE initialize_solution
344 !*****
345 !*
346 !*
347 !*****
348 SUBROUTINE print_to_file(C,file_name,N,DX)
349   IMPLICIT NONE
350
351   REAL, INTENT(IN) :: C(N),DX
352   INTEGER, INTENT(IN) :: N
353
354   CHARACTER* (*), INTENT(IN) :: file_name
355
356   INTEGER :: I
357   INTEGER :: FILE_ID
358   PARAMETER(FILE_ID=999)
359   REAL :: current_position
360
361   OPEN(UNIT=FILE_ID, file=file_name)
362
363   current_position = 0;
364   DO I=1,N
365
366     WRITE( UNIT=FILE_ID, FMT=* ) current_position ,'\t', C(I)
367     current_position = current_position + DX
368
369   END DO
370
371   CLOSE(FILE_ID)
372
373 END SUBROUTINE print_to_file
374 !*****
375 !*
376 !*

```

```

377 !*
378 !*****
379 SUBROUTINE init_A_matrix(A,K,N)
380   IMPLICIT NONE
381
382   INTEGER, INTENT(IN) ::N
383   REAL, INTENT(IN) ::K
384   REAL, INTENT(OUT) ::A(N,N)
385
386   INTEGER ::I
387
388   DO I = 2,N-1
389     A(I,I-1) = -K
390     A(I,I) = 1
391     A(I,I+1) = K
392   END DO
393
394   A(1,1) = 1
395   A(N,N) = 1
396
397 END SUBROUTINE init_A_matrix
398 !*****
399 !*
400 !*
401 !*****
402 SUBROUTINE solve_thomas_algorithm(N,aa,b,c,old_c,new_c)
403   IMPLICIT NONE
404
405   REAL, INTENT(IN) :: aa(N),b(2:N),c(N-1),old_c(N)
406   INTEGER, INTENT(IN) :: N
407   REAL, INTENT(INOUT) :: new_c(N)
408
409   INTEGER :: I
410   REAL :: alpha(N),beta(2:N),g(N)
411
412   alpha(1) = aa(1)
413   DO I=2,N
414     beta(I)=b(I)/alpha(I-1)
415     alpha(I)=aa(I) -beta(I)*c(I-1)
416   END DO
417
418   g(1)=old_c(1)
419   DO I=2,N
420     g(I)=old_c(I) -beta(I)*g(I-1)
421   END DO
422
423   new_c(N)=g(N)/alpha(N)
424   DO I=N-1,1,-1
425     new_c(I)=(g(I) -c(I)*new_c(I+1))/alpha(I)
426   END DO
427
428 END SUBROUTINE solve_thomas_algorithm
429 !*****
430 !*
431 !*
432 !*****
433 REAL FUNCTION speed(MODE,time)
434   IMPLICIT NONE
435
436   INTEGER, INTENT(IN) :: MODE
437   REAL, INTENT(IN) :: time
438
439   IF( MODE == 1 ) THEN
440     speed=2.0
441   ELSE
442     speed=time/20.0
443   END IF
444
445 END FUNCTION speed
446 !*****
447 !*
448 !*
449 !*****
450 SUBROUTINE take_one_snap_shot(mode,method,TIME,N,C,DX)
451   IMPLICIT NONE

```

```

453 INTEGER, INTENT(IN) :: TIME,mode,method,N
454 REAL, INTENT(IN) :: C(N),DX
455
456 IF (TIME==15) THEN
457   SELECT CASE(method)
458   CASE(1)
459     IF(mode==1) THEN
460       CALL print_to_file(C,'exp15.txt',N,DX)
461     ELSE
462       CALL print_to_file(C,'exp_extra15.txt',N,DX)
463     END IF
464   CASE(2)
465     IF(mode==1) THEN
466       CALL print_to_file(C,'lax15.txt',N,DX)
467     ELSE
468       CALL print_to_file(C,'lax_extra15.txt',N,DX)
469     ENDIF
470   CASE(3)
471     IF(mode==1) THEN
472       CALL print_to_file(C,'imp15.txt',N,DX)
473     ELSE
474       CALL print_to_file(C,'imp_extra15.txt',N,DX)
475     END IF
476   CASE(4)
477     IF(mode==1) THEN
478       CALL print_to_file(C,'cr15.txt',N,DX)
479     ELSE
480       CALL print_to_file(C,'cr_extra15.txt',N,DX)
481     END IF
482   END SELECT
483 ELSE
484   SELECT CASE(method)
485   CASE(1)
486     IF(mode==1) THEN
487       CALL print_to_file(C,'exp30.txt',N,DX)
488     ELSE
489       CALL print_to_file(C,'exp_extra30.txt',N,DX)
490     END IF
491   CASE(2)
492     IF(mode==1) THEN
493       CALL print_to_file(C,'lax30.txt',N,DX)
494     ELSE
495       CALL print_to_file(C,'lax_extra30.txt',N,DX)
496     ENDIF
497   CASE(3)
498     IF(mode==1) THEN
499       CALL print_to_file(C,'imp30.txt',N,DX)
500     ELSE
501       CALL print_to_file(C,'imp_extra30.txt',N,DX)
502     END IF
503   CASE(4)
504     IF(mode==1) THEN
505       CALL print_to_file(C,'cr30.txt',N,DX)
506     ELSE
507       CALL print_to_file(C,'cr_extra30.txt',N,DX)
508     END IF
509   END SELECT
510 END IF
511 END SUBROUTINE take_one_snap_shot
512 !*****
513 !*
514 !*
515 !*****
516 REAL FUNCTION RMS(CEXACT,C,N)
517   IMPLICIT NONE
518
519   REAL, INTENT(IN) :: CEXACT(N),C(N)
520   INTEGER, INTENT(IN) :: N
521
522   INTEGER :: I
523
524   RMS=0.
525   DO I=1,N
526     RMS = RMS+(CEXACT(I)-C(I))**2
527   END DO
528

```

```

529   RMS = RMS/N
530   RMS = SQRT(RMS)
531 END FUNCTION RMS
532 !*****
533 !*
534 !*
535 !*****
536 SUBROUTINE get_current_exact_solution(CEXACT,N,current_first_limit,DX)
537   IMPLICIT NONE
538   REAL, INTENT(IN)      :: current_first_limit,DX
539   REAL, INTENT(OUT)    :: CEXACT(0:N-1)
540   INTEGER, INTENT(IN)  :: N
541
542   INTEGER :: I
543   REAL :: first_limit
544   REAL :: second_limit
545   REAL :: av,R,shift,x,PI
546
547   PARAMETER( PI = ACOS(-1.) )
548
549   first_limit = 25.0
550   second_limit = 35.0
551
552   shift = current_first_limit - FIRST_LIMIT
553   first_limit = current_first_limit
554   second_limit = second_limit + shift
555
556   av = (second_limit+first_limit)/2.0
557   R = av - first_limit
558
559   CEXACT = 0.
560   x = 0.
561   DO I = 0,N-1
562
563     IF( x ≥ first_limit .AND. x ≤ second_limit ) THEN
564       CEXACT(I) = 1 + COS( PI * (x -av)/R )
565     END IF
566
567     x = x + DX
568   END DO
569 END SUBROUTINE get_current_exact_solution

```

7 References

1. Numerical Methods for physics. Second edition. Alejandro Garcia
2. Applied Numerical Methods for Engineers. Terrence Akal.
3. Computational Techniques for fluid dynamics. Second edition. C.A.J.Fletcher