

① Practice Midterm  
4.34

find  $\alpha \rightarrow \phi_1^T M \phi_2 = 0$  Modes must be  $\perp$

$$\begin{bmatrix} 1 & 0.414 \end{bmatrix} \begin{bmatrix} 3 & 1 \\ 1 & 1 \end{bmatrix} \begin{bmatrix} 1 \\ \alpha \end{bmatrix} =$$

$$= \begin{bmatrix} 1 & 0.414 \end{bmatrix} \begin{bmatrix} 3+\alpha \\ 1+\alpha \end{bmatrix} = 3+\alpha + 0.414 + 0.414\alpha$$

$$= 3.414 + 1.414\alpha$$

$$\boxed{\alpha = -\frac{3.414}{1.414} = -2.414}$$

Mass Normalize: (Wouldn't have all this arithmetic on final)

$$\begin{bmatrix} 1 & 0.414 \end{bmatrix} \begin{bmatrix} 3 & 1 \\ 1 & 1 \end{bmatrix} \begin{bmatrix} 1 \\ 0.414 \end{bmatrix} = \begin{bmatrix} 1 & 0.414 \end{bmatrix} \begin{bmatrix} 3.414 \\ 1.414 \end{bmatrix}$$

$$= 3.414 + 1.414 \cdot 0.414 = \mu_1$$

$$\begin{bmatrix} 1 & -2.414 \end{bmatrix} \begin{bmatrix} 3 & 1 \\ 1 & 1 \end{bmatrix} \begin{bmatrix} 1 \\ -2.414 \end{bmatrix} = \begin{bmatrix} 1 & -2.414 \end{bmatrix} \begin{bmatrix} 3-2.414 \\ 1-2.414 \end{bmatrix} = \mu_2$$

$$\{\Phi\} = \{\phi_i\} \frac{1}{\sqrt{\mu_i}} \text{ etc...}$$

$$\ddot{n}_1 + \omega_n^2 n_1 = \{\Phi_1\}^T \begin{Bmatrix} 0 \\ 20x \end{Bmatrix} = \frac{0.414 \cdot 20x}{\sqrt{\mu_1}} = c_1 x \quad \left. \vphantom{\ddot{n}_1} \right\} \text{Ramp}$$

$$\ddot{n}_2 + \omega_n^2 n_2 = \{\Phi_2\}^T \begin{Bmatrix} 0 \\ 20x \end{Bmatrix} = c_2 x$$

$$n_1(x) = \frac{c_1}{\omega_1^3} [\omega_1 x - \sin(\omega_1 x)] h(x) - \text{App. B for } \xi = 0$$

$$n_2(x) = \frac{c_2}{\omega_2^3} [\omega_2 x - \sin(\omega_2 x)] h(x)$$

$$y = [\Phi] \begin{Bmatrix} n_1(x) \\ n_2(x) \end{Bmatrix} \dots$$

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## ② Practice Midterm

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Non-dimensionalize  $\rightarrow x' = \omega_n x$ ,  $\omega_n = \sqrt{\frac{mg \frac{L}{2}}{\frac{1}{3} mL^2}} = \sqrt{\frac{3g}{2L}}$

$$\begin{bmatrix} 1 & 0 \\ 0 & 1 \end{bmatrix} \begin{Bmatrix} \theta_1'' \\ \theta_2'' \end{Bmatrix} + \begin{bmatrix} \alpha + 0.5 & -\alpha \\ -\alpha & \alpha + 0.5 \end{bmatrix} \begin{Bmatrix} \theta_1 \\ \theta_2 \end{Bmatrix} = 0$$

EVP

$$\begin{bmatrix} \alpha + 0.5 - \omega^2 & -\alpha \\ -\alpha & \alpha + 0.5 - \omega^2 \end{bmatrix} \begin{Bmatrix} \phi_1 \\ \phi_2 \end{Bmatrix} = 0$$

non-trivial if matrix is singular  $\rightarrow \det = 0$

$$(\alpha + 0.5 - \omega^2)(\alpha + 0.5 - \omega^2) - \alpha^2 = 0$$

$$\cancel{\alpha^2} + 0.5\alpha - \alpha\omega^2 + 0.5\alpha + 0.25 - 0.5\omega^2 - \alpha\omega^2 - 0.5\omega^2 + \omega^4 - \cancel{\alpha^2} = 0$$

$$\omega^4 - 2(\alpha + 0.5)\omega^2 + 0.25 + \alpha = 0$$

$$\omega^2 = \frac{2(\alpha + 0.5) \pm \sqrt{4(\alpha + 0.5)^2 - 4(1)(0.25 + \alpha)}}{2}$$

$$\begin{aligned} \omega^2 &= (\alpha + 0.5) \pm \sqrt{(\alpha + 0.5)^2 - (\alpha + 0.25)} \\ &= (\alpha + 0.5) \pm \sqrt{\alpha^2 + \alpha + 0.25 - \alpha - 0.25} \\ &= (\alpha + 0.5) \pm \alpha = \end{aligned}$$

$$\boxed{\omega_1^2 = 0.5, \omega_2^2 = 0.5 + 2\alpha}$$

for small  $\alpha$  -  $\omega_1 \approx \omega_2$

Modes  $\rightarrow$

$$\begin{bmatrix} \alpha & -\alpha \\ -\alpha & \alpha \end{bmatrix} \phi_1 = 0 \quad \phi_1 = \begin{Bmatrix} 1 \\ 1 \end{Bmatrix}$$

$$\begin{bmatrix} -\alpha & -\alpha \\ -\alpha & -\alpha \end{bmatrix} \phi_2 = 0 \quad \phi_2 = \begin{Bmatrix} 1 \\ -1 \end{Bmatrix}$$

Given an initial condition,

$$n_1(x) = \text{Re}(N_1 e^{i\omega_1 t})$$

$$n_2(x) = \text{Re}(N_2 e^{i\omega_2 t})$$

} No decay  $\rightarrow$  damping neglected

$$\{\delta\} = [\ddot{\Phi}] \begin{Bmatrix} n_1(x) \\ n_2(x) \end{Bmatrix} \rightarrow$$

(2-cont.)

$$y_1 = \frac{1}{\sqrt{u_1}} n_1(x) + \frac{1}{\sqrt{u_2}} n_2(x)$$

$$y_2 = \frac{1}{\sqrt{u_1}} n_1(x) + \frac{-1}{\sqrt{u_2}} n_2(x)$$

$y_1(x)$  is the sum of 2 harmonics with nearly equal amplitudes and nearly the same frequency, so beating occurs

$$y_1 \approx \text{Re}(A e^{i\Delta\omega t}) \text{Re}(A e^{i\omega_{ave} t}) \quad (\text{see below})$$

$$\text{Wave} = (\sqrt{0.5} + \sqrt{0.5 + 2\alpha}) \frac{1}{2} \quad (\alpha \text{ has little effect here.)}$$

$$\Delta\omega = (\sqrt{0.5 + 2\alpha} - \sqrt{0.5}) \frac{1}{2}$$

depends on  $\alpha$

could solve this on calculator iteratively to find  $\alpha$  for known  $\Delta\omega$

This part is little intricate for an exam

for small  $\alpha \sim$  Taylor series

$$\frac{\partial \Delta\omega}{\partial \alpha} = (0.5 + 2\alpha)^{-1/2} \left(\frac{1}{2}\right) (2) \Big|_{\alpha=0} = \frac{1}{\sqrt{0.5}}$$

$$\Delta\omega = 0 + \frac{\partial \Delta\omega}{\partial \alpha} \alpha = \sqrt{2} \alpha$$

$$\Delta\omega = \frac{2\pi}{T} = \frac{2\pi}{63.2} \sim 2 \text{ beats per period } \checkmark$$

$$\Delta\omega = \frac{\pi}{63} = \sqrt{2} \alpha$$

$$\alpha \approx \frac{\pi}{63\sqrt{2}} \approx 0.035 \quad (\text{True } \alpha = 0.036605)$$

Or, if you need to derive the beating equation above:

$$y_1 = \text{Re}(c_1 e^{i\omega_1 t}) + \text{Re}(c_2 e^{i\omega_2 t}) \quad \text{for } c_1 = c_2$$

$$y_1 = c_1 \left[ \text{Re}(e^{i\omega_{ave} t} e^{-i\Delta\omega t} + e^{i\omega_{ave} t} e^{i\Delta\omega t}) \right]$$

$$= \frac{1}{2} c_1 \left[ e^{i\omega_{ave} t} e^{-i\Delta\omega t} + e^{-i\omega_{ave} t} e^{i\Delta\omega t} + e^{i\omega_{ave} t} e^{i\Delta\omega t} + e^{-i\omega_{ave} t} e^{-i\Delta\omega t} \right]$$

$$y_1 = \frac{1}{2} c_1 \left[ e^{i\omega_{ave} t} (e^{i\Delta\omega t} + e^{-i\Delta\omega t}) + e^{-i\omega_{ave} t} (e^{i\Delta\omega t} + e^{-i\Delta\omega t}) \right]$$

equation for beating

$2\cos(\Delta\omega t)$  - Factor out

(3)

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$$a) \rightarrow \{x(t)\} = \text{Re}\{\{X\} e^{i\omega t}\} \rightarrow y(t) = \text{Re}\{Y e^{i\omega t}\} \rightarrow$$

$$\{X\} = [K + i\omega c - \omega^2 m]^{-1} \begin{Bmatrix} K \\ 0 \end{Bmatrix} Y$$

$$= \begin{bmatrix} K + i\omega c - \omega^2 m & -i\omega c \\ -i\omega c & 2K + i\omega c - \omega^2 m \end{bmatrix}^{-1} \begin{Bmatrix} K \\ 0 \end{Bmatrix} Y$$

use  $\omega = \omega_1 \rightarrow$  find  $\omega_1$

$$\left| [K - \omega^2 m] \right| = \left| \begin{bmatrix} K - m\omega^2 & \\ & 2K - m\omega^2 \end{bmatrix} \right|$$

by inspection (diagonal system)  $\rightarrow \omega_1 = \sqrt{K/m}, \omega_2 = \sqrt{2K/m}$

$$\rightarrow = \begin{bmatrix} K + i\omega c - (K/m) \cdot m & -i\omega c \\ -i\omega c & K + i\omega c \end{bmatrix}^{-1} \begin{Bmatrix} K \\ 0 \end{Bmatrix} Y$$

$$= \begin{bmatrix} K + i\omega c & i\omega c \\ i\omega c & i\omega c \end{bmatrix} \frac{1}{(K + i\omega c)i\omega c - (i\omega c)^2} \begin{Bmatrix} K \\ 0 \end{Bmatrix} Y$$

$$= \begin{bmatrix} (K + i\omega c)K & \\ K(i\omega c) & \end{bmatrix} \frac{1}{K(i\omega c)} Y$$

$$= \begin{bmatrix} \frac{K^2 + i\omega c K}{i\omega c K} & \\ & 1 \end{bmatrix} Y$$

b) General case:

$$\{X\} = \begin{bmatrix} 2K + i\omega c - \omega^2 m & i\omega c \\ i\omega c & K + i\omega c - \omega^2 m \end{bmatrix} \frac{1}{\det(\cdot)} \begin{Bmatrix} K \\ 0 \end{Bmatrix} Y$$

$$= \begin{Bmatrix} 2K + i\omega c - \omega^2 m \\ i\omega c \end{Bmatrix} \frac{K}{\det(\cdot)} Y$$

$x_2$  cannot = 0 unless  $c = 0$

$$x_1 \rightarrow 2K + i\omega c - \omega^2 m = 0$$

$$\omega = \frac{-ic \pm \sqrt{-c^2 - 4(-m)(2K)}}{-2m}$$

solution for  $\omega$  is imaginary unless  $c = 0$

$\rightarrow$  so there is no real  $\omega$  for which  $x_1 = 0$

3-cont.

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c) from previous

$$\begin{Bmatrix} \bar{x}_1 \\ \bar{x}_2 \end{Bmatrix} = \begin{bmatrix} i\omega c & i\omega c \\ i\omega c & i\omega c \end{bmatrix} \frac{1}{\underline{0}} \begin{Bmatrix} k \\ 0 \end{Bmatrix} \Phi$$

$$\bar{x}_1, \bar{x}_2 \rightarrow \infty$$

Explanation  $\rightarrow$  equal nat freq's

$$[[K] - \omega^2 [M]] \{\phi\} = 0$$

$$\begin{bmatrix} 0 & 0 \\ 0 & 0 \end{bmatrix} \{\phi\} = 0 \rightarrow \phi \text{ is arbitrary!}$$

$$\text{if } \phi_1 = \begin{Bmatrix} 1 \\ 1 \end{Bmatrix} \text{ then } \{\phi_1\}^T [C] \{\phi_1\} =$$

$$\begin{bmatrix} 1 & 1 \end{bmatrix} \begin{bmatrix} c & -c \\ -c & c \end{bmatrix} \begin{Bmatrix} 1 \\ 1 \end{Bmatrix} = \begin{bmatrix} 1 & 1 \end{bmatrix} \begin{Bmatrix} 0 \\ 0 \end{Bmatrix} = 0$$

$$\text{so, } 2\xi_1 \omega_1 = 0, \xi_1 = 0$$

so this mode is undamped and it's response approaches  $\infty$  when it is forced at it's nat. freq.

d) given  $x_1 = \text{Re}(A e^{i\omega t}) \rightarrow$  use 2nd EOM

$x_2$  must also be harmonic  $\rightarrow x_2 = \text{Re}(X_2 e^{i\omega t})$

$$m\ddot{x}_2 + c\dot{x}_2 - c\dot{x}_1 + k_2 x_2 = 0$$

$$\bar{X}_2 = \frac{i\omega c \bar{X}_1}{k + i\omega c - \omega^2 m}$$

$$\bar{X}_2 = \frac{i\omega c A}{k + i\omega c - \omega^2 m}$$

$$x_2(t) = \text{Re}(\bar{X}_2 e^{i\omega t})$$

**E.C** preload  $\sim$

$$\left. \begin{array}{l} \downarrow mg \\ \uparrow k_2 \\ \uparrow k_2 \Delta_0 \end{array} \right\} \begin{array}{l} k_2 \Delta_0 - mg = 0 \\ \Delta_0 = \frac{mg}{k_2} \end{array}$$

loses contact if  $\Delta > \Delta_0$

$$\Delta = x_1 - y$$

$$\boxed{x_1 - y > \frac{mg}{k}}$$

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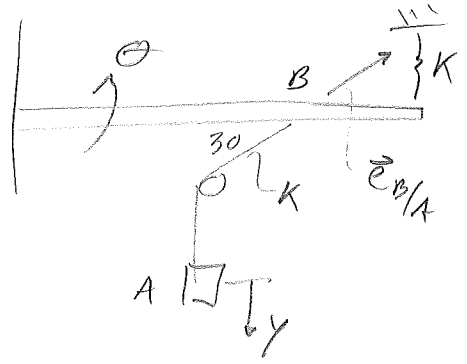
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4

Find EOM  $\theta_1 = \theta$   $\theta_2 = y$

$$T = \frac{1}{2} \left( \frac{1}{3} mL^2 \right) \dot{\theta}^2 + \frac{1}{2} 3m \dot{y}^2$$

$\rightarrow$  0 K for <sup>I about pin</sup> pure rotation, otherwise use  $\frac{1}{2} m v_g^2$  and  $\frac{1}{2} I_g \dot{\theta}^2$



$$M = \begin{bmatrix} \frac{1}{3} mL^2 & 0 \\ 0 & 3m \end{bmatrix} \text{ for } \begin{Bmatrix} \ddot{\theta} \\ \ddot{y} \end{Bmatrix}$$

$$V = \frac{1}{2} K \Delta_1^2 + \frac{1}{2} K \Delta_2^2$$

$$\Delta_1 = L\theta$$

$$\Delta_2 = u_a - u_b \text{ - stiff spring approx / linearization}$$

$$= y - (\cos 30 i + \sin 30 j) \cdot \left( \frac{L}{2} \theta \hat{j} \right)$$

$$= y - \frac{L}{2} \sin 30 \theta$$

$$V = \frac{1}{2} KL^2 \theta^2 + \frac{1}{2} K \left( y^2 + 2 \cdot \frac{L}{2} \sin 30 \theta y + \frac{L^2}{4} \sin^2 30 \theta^2 \right)$$

$$K = \begin{bmatrix} KL^2 & -\frac{KL}{2} \sin 30 \\ -\frac{KL}{2} \sin 30 & \frac{KL^2}{4} \sin^2 30 \end{bmatrix}$$

$$\checkmark \sim I_0 \ddot{\theta} + KL^2 \theta - \frac{KL}{2} \sin 30 y = 0$$

$\theta = 0, y \geq 0 \sim$  oops - sign error on y - not consistent w  $\hat{e}_{B/A}$

$$K = \begin{bmatrix} KL^2 & +\frac{KL}{2} \sin 30 \\ +\frac{KL}{2} \sin 30 & \frac{KL^2}{4} \sin^2 30 \end{bmatrix}$$

$$Pin = \dot{y} \cdot F$$

$$Q = \begin{Bmatrix} 0 \\ F \end{Bmatrix} \Rightarrow \begin{bmatrix} \frac{1}{3} mL^2 & 0 \\ 0 & 3m \end{bmatrix} \begin{Bmatrix} \ddot{\theta} \\ \ddot{y} \end{Bmatrix} + \begin{bmatrix} KL^2 & \frac{KL}{2} \sin 30 \\ \frac{KL}{2} \sin 30 & \frac{KL^2}{4} \sin^2 30 \end{bmatrix} \begin{Bmatrix} \theta \\ y \end{Bmatrix} = \begin{Bmatrix} 0 \\ F \end{Bmatrix}$$

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