

HW 4, ME 440 Intermediate Vibration, Fall 2017

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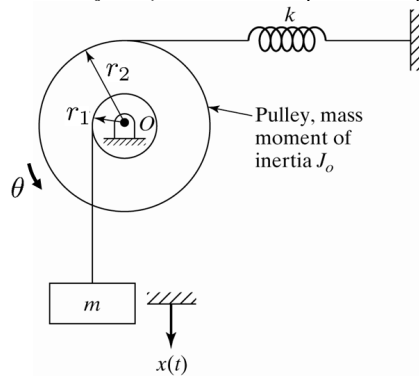
December 30, 2019

0.1 Problem 1

Problem 1

The pulley is in fixed axis rotation about Point O . Using energy concepts and θ as the generalized coordinate, determine

- the natural frequency of the system shown below, and
- the equation of motion for the system, in terms of the parameters provided.



0.1.1 Part a

Using Rayleigh method, we need to find T_{\max} and U_{\max} where T is the kinetic energy of the system and U is the potential energy and then solve for ω_n by setting $T_{\max} = U_{\max}$.

Kinetic energy is

$$T = \frac{1}{2}m\dot{x}^2 + \frac{1}{2}J_o\dot{\theta}^2$$

But $x = r_1\theta$, therefore $\dot{x} = r_1\dot{\theta}$ and the above becomes

$$T = \frac{1}{2}m(r_1\dot{\theta})^2 + \frac{1}{2}J_o\dot{\theta}^2 \quad (1)$$

And potential energy only comes from the spring, since we assume x is measured from static equilibrium. Hence

$$\begin{aligned} U &= \frac{1}{2}kx^2 \\ &= \frac{1}{2}k(r_2\theta)^2 \end{aligned} \quad (2)$$

To get ω_n into (1) and (2), we now assume that motion is harmonic, hence $\theta = \theta_{\max} \sin(\omega_n t)$, Therefore $\dot{\theta} = \theta_{\max} \omega_n \cos(\omega_n t)$ and rewriting (1,2) using these expressions results in

$$\begin{aligned} T &= \frac{1}{2}m(r_1\theta_{\max}\omega_n \cos(\omega_n t))^2 + \frac{1}{2}J_o(\theta_{\max}\omega_n \cos(\omega_n t))^2 \\ U &= \frac{1}{2}k(r_2(\theta_{\max} \sin(\omega_n t)))^2 \end{aligned}$$

Hence, maximum is when $\theta = \theta_{\max}$ and $\dot{\theta} = \theta_{\max}\omega_n$ and the above becomes

$$T_{\max} = \frac{1}{2}mr_1^2\theta_{\max}^2\omega_n^2 + \frac{1}{2}J_o\theta_{\max}^2\omega_n^2$$

$$U_{\max} = \frac{1}{2}kr_2^2\theta_{\max}^2$$

Now

$$T_{\max} = U_{\max}$$

$$\frac{1}{2}mr_1^2\theta_{\max}^2\omega_n^2 + \frac{1}{2}J_o\theta_{\max}^2\omega_n^2 = \frac{1}{2}kr_2^2\theta_{\max}^2$$

$$mr_1^2\omega_n^2 + J_o\omega_n^2 = kr_2^2$$

Hence

$$\omega_n^2 = \frac{kr_2^2}{mr_1^2 + J_o}$$

$$\omega_n = \sqrt{\frac{kr_2^2}{mr_1^2 + J_o}}$$

0.1.2 Part b

The equation of motion is given by

$$\frac{d}{dt}(T + U) = 0$$

We found T, U in part (a), therefore the above becomes

$$\frac{d}{dt}\left(\frac{1}{2}m(r_1\dot{\theta})^2 + \frac{1}{2}J_o\dot{\theta}^2 + \frac{1}{2}k(r_2\theta)^2\right) = 0$$

$$mr_1^2\dot{\theta}\ddot{\theta} + J_o\dot{\theta}\ddot{\theta} + kr_2^2\theta\dot{\theta} = 0$$

For non trivial motion $\dot{\theta} \neq 0$ for all time, hence we can divide throughout by $\dot{\theta}$ and obtain

$$mr_1^2\ddot{\theta} + J_o\ddot{\theta} + kr_2^2\theta = 0$$

$$\ddot{\theta}(mr_1^2 + J_o) + kr_2^2\theta = 0$$

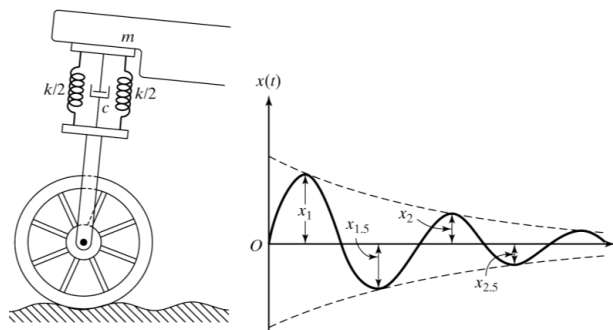
$$\ddot{\theta} + \frac{kr_2^2}{mr_1^2 + J_o}\theta = 0$$

The above is the equation of motion.

0.2 Problem 2

Problem 2

An underdamped shock absorber is to be designed for motorcycle of mass 200 kg. When the shock absorber is subjected to an initial vertical velocity due to a road bump, the resulting displacement-time curve is to be as illustrated below. Determine the necessary stiffness and damping constants of the shock absorber if the damped period of vibration is to be 2 seconds and the amplitude x_i is to be reduced to $1/4$ in one half cycle (i.e., $x_{1.5} = x_i/4$). Also find the minimum initial velocity that leads to a maximum displacement of 250 mm.



First part

The first step is to determine damping ratio ζ . This is done using logarithmic decrement.

Since $X_{1.5} = \frac{1}{4}X_1$ and $X_2 = \frac{1}{4}X_{1.5}$ then

$$\begin{aligned} X_2 &= \frac{1}{4} \left(\frac{1}{4} X_1 \right) \\ &= \frac{1}{16} X_1 \end{aligned}$$

Using

$$\frac{X_1}{X_2} = \frac{e^{-\zeta\omega_n t_1}}{e^{-\zeta\omega_n(t_1+t_2)}}$$

Where $t_2 = t_1 + \tau_d$ and τ_d is damped period. Therefore the above becomes

$$\begin{aligned} \frac{X_1}{\frac{1}{16}X_1} &= \frac{e^{-\zeta\omega_n t_1}}{e^{-\zeta\omega_n(t_1+\tau_d)}} = \frac{e^{-\zeta\omega_n t_1}}{e^{-\zeta\omega_n t_1} e^{-\zeta\omega_n \tau_d}} = e^{\zeta\omega_n \tau_d} \\ \ln(16) &= \zeta\omega_n \tau_d \end{aligned}$$

Taking log of both sides gives

$$\ln(16) = \zeta\omega_n \tau_d \quad (1)$$

But

$$\begin{aligned} \tau_d &= \frac{2\pi}{\omega_d} \\ &= \frac{2\pi}{\omega_n \sqrt{1-\zeta^2}} \end{aligned}$$

And (1) simplifies to

$$\begin{aligned} \ln(16) &= \zeta\omega_n \frac{2\pi}{\omega_n \sqrt{1-\zeta^2}} \\ 2.7726 &= \frac{2\pi\zeta}{\sqrt{1-\zeta^2}} \end{aligned}$$

Squaring both sides and solving for ζ gives

$$\begin{aligned} (2.7726)^2 (1-\zeta^2) &= 4\pi^2 \zeta^2 \\ \zeta^2 (4\pi^2 + 7.6873) &= 7.6873 \\ \zeta^2 &= \frac{7.6873}{4\pi^2 + 7.6873} \end{aligned}$$

Taking the positive root results in

$$\begin{aligned} \zeta &= \sqrt{\frac{7.6873}{4\pi^2 + 7.6873}} \\ &= 0.40371 \end{aligned}$$

Now that ζ is know, ω_n can be found, since we are told that $\tau_d = 2$ seconds. Using

$$\tau_d = \frac{2\pi}{\omega_n \sqrt{1-\zeta^2}}$$

Then solving for ω_n from the above gives

$$\begin{aligned} 2 &= \frac{2\pi}{\omega_n \sqrt{1-0.40371^2}} \\ \omega_n &= \frac{\pi}{\sqrt{1-0.40371^2}} \\ &= 3.4339 \text{ rad/sec} \end{aligned}$$

Now we are ready to find the stiffness coefficient k and damping coefficient c . Using

$$\zeta = \frac{c}{2\omega_n m}$$

Then

$$\begin{aligned} c &= 2\zeta\omega_n m \\ &= 2(0.40371)(3.4339)(200) \\ &= 554.52 \text{ N-s/m} \end{aligned}$$

But since

$$\omega_n^2 = \frac{k}{m}$$

Then k is now found

$$\begin{aligned} k &= \omega_n^2 m \\ &= (3.4339)^2 (200) \\ &= 2358.3 \text{ N/m} \end{aligned}$$

Second part

Maximum displacement occurs at time t_1 as given by (from textbook)

$$\sin \omega_d t_1 = \sqrt{1 - \zeta^2}$$

Hence

$$\begin{aligned} \omega_d t_1 &= \arcsin(\sqrt{1 - \zeta^2}) \\ t_1 &= \frac{1}{\omega_n \sqrt{1 - \zeta^2}} \arcsin(\sqrt{1 - \zeta^2}) \\ &= \frac{1}{3.4339 \sqrt{1 - 0.40371^2}} \arcsin(\sqrt{1 - 0.40371^2}) \\ &= 0.36772 \text{ sec} \end{aligned}$$

Since

$$x(t) = X e^{-\zeta\omega_n t} \sin(\omega_d t) \quad (2)$$

Then at maximum displacement, where $x = 0.25$ m, the above becomes

$$\begin{aligned} x_{\max}(t_1) &= X e^{-\zeta\omega_n t_1} \sin(\omega_d t_1) \\ \frac{x_{\max} e^{\zeta\omega_n t_1}}{\sin(\omega_d t_1)} &= X \end{aligned}$$

Plug-in numerical values to solve for maximum displacement X gives

$$\begin{aligned} X &= \frac{0.25 \exp(0.40371 \times 3.4339 \times 0.36772)}{\sin((3.4339 \sqrt{1 - 0.40371^2})(0.36772))} \\ &= 0.45495 \text{ m} \end{aligned}$$

From (2), the velocity is found

$$\begin{aligned} \dot{x}(t) &= -\zeta\omega_n X e^{-\zeta\omega_n t} \sin(\omega_d t) + X e^{-\zeta\omega_n t} \omega_d \cos(\omega_d t) \\ &= X e^{-\zeta\omega_n t} (\omega_d \cos(\omega_d t) - \zeta\omega_n \sin(\omega_d t)) \end{aligned}$$

At $t = 0$ the above gives

$$\begin{aligned} \dot{x}(0) &= X\omega_d \\ &= X(\omega_n \sqrt{1 - \zeta^2}) \end{aligned}$$

Plug-in in numerical values

$$\begin{aligned} \dot{x}(0) &= 0.45495 (3.4339 \sqrt{1 - 0.40371^2}) \\ &= 1.4293 \text{ m/s} \end{aligned}$$