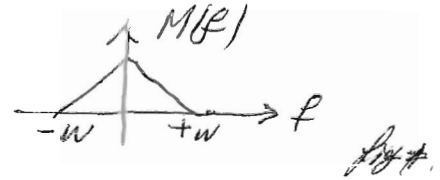


Drill Prob. # 3.4) $V_2(t) = a_1 v_1(t) + a_2 v_1^2(t)$ (1), $v_1(t) = A_c \cos(2\pi f_c t) + m(t)$ (2)

$$V_2(t) = a_1 A_c \cos(2\pi f_c t) + a_1 m(t) + a_2 A_c^2 \cos^2(2\pi f_c t) + a_2 m^2(t) + 2 a_2 A_c m(t) \cos(2\pi f_c t) \quad (3)$$

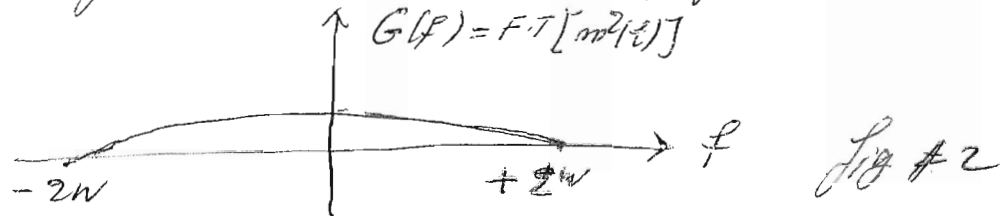
Assume $M(f)$ has the following form:



Let $g(t) \triangleq m^2(t) = m(t) \cdot m(t)$

$\Rightarrow G(f) = M(f) \otimes M(f)$ The spectrum of $g(t) = m^2(t)$

Will extend from $-2W$ to $2W$ Hz, for example would be



Note: If you want to find $G(f)$, then you have

to do $G(f) = \int_{-\infty}^{+\infty} M(x) M(f-x) dx$. We are not interested to find the exact equation of $G(f)$, all we need to know is that the spectrum of $G(f) = F.T[m^2(t)]$ will extend from $-2W$ to $2W$ Hz.

Let us to take the F.T of eq(3) and plot it!

$$V_2(t) = a_1 A_c \cos(2\pi f_c t) + a_1 m(t) + \frac{a_2 A_c^2}{2} [1 + \cos(4\pi f_c t)] + a_2 m^2(t) + 2 a_2 A_c m(t) \cos(2\pi f_c t) \quad (4)$$

$$\Rightarrow V_2(f) = \frac{a_1 A_c}{2} [\delta(f-f_c) + \delta(f+f_c)] + a_1 M(f) + \frac{a_2 A_c^2}{2} \delta(f) + \frac{a_2 A_c^2}{4} [\delta(f-2f_c) + \delta(f+2f_c)] + a_2 \underbrace{F.T[m^2(t)]}_{G(f)} + a_2 A_c [M(f-f_c) + M(f+f_c)] \quad (5)$$

The plot of eq. (5) is shown in Figure # 3.

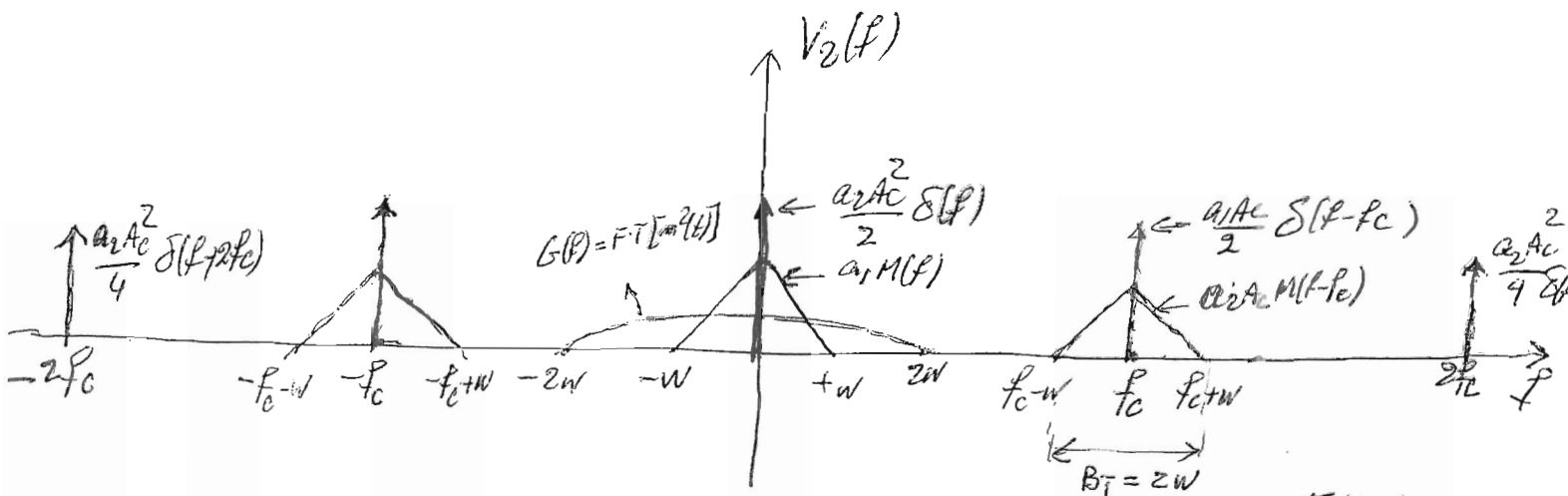


Fig # 3

Fig # 3 shows the spectral content of $V_2(f)$.

1) To extract the desired AM signal, use eq (4) and identify the AM signal:

$$V_2(t) = \underbrace{a_1 A_c \left[1 + \frac{2a_2}{a_1} m(t) \right] \cos 2\pi f_c t}_{\text{Desired AM signal}} + \underbrace{\left(a_1 m(t) + a_2 m^2(t) + \frac{a_2 A_c^2}{2} \cos 4\pi f_c t \right)}_{\text{Undesired component}} \quad (6)$$

A Bandpass filter centered at f_c with total extend of $2W$, That is having a transfer function of :

$$H(f) = \text{rect}\left(\frac{f-f_c}{2W}\right) + \text{rec}\left(\frac{f+f_c}{2W}\right) \quad (7)$$

will pass the desired signal (AM signal) and eliminated the unwanted components.

Using eq. (7) and figure # (3) we see that the required B.P.F must have a bandwidth of $2W$ Hz and centered at f_c , thus the cut-off frequencies of BPF are $f_c - W$ and $f_c + W$ Hz.

c) To avoid spectral overlapping of the desired signal (AM signal) with that of unwanted signals in $V_d(t)$, using figure # 3, we see that

$$\left. \begin{aligned} 1) f_c - W &\geq 2W \Rightarrow f_c \geq 3W \\ 2) f_c + W &\leq 2f_c \Rightarrow f_c \geq W \end{aligned} \right\} \text{Thus } f_c > 3W$$

3.23

Assume $m(t)$ with spectrum of

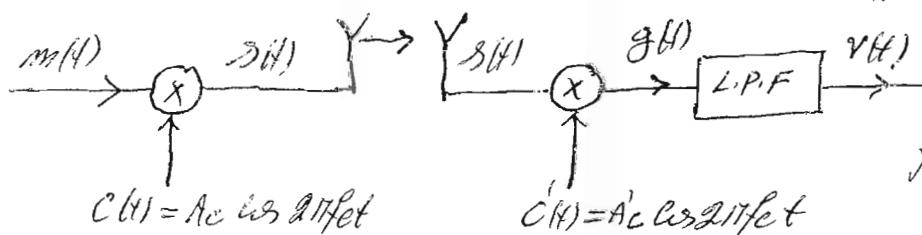
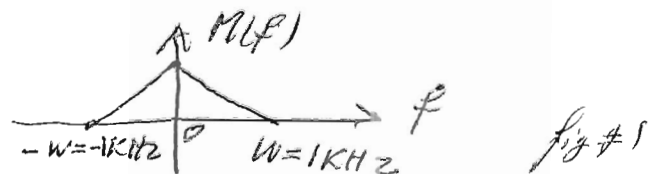


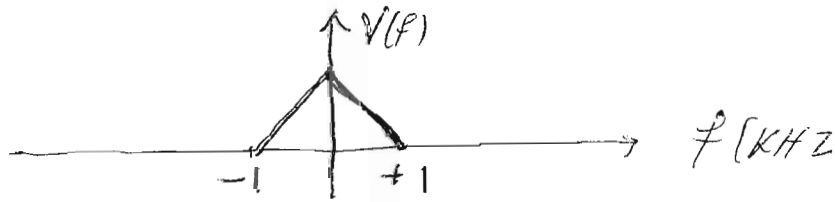
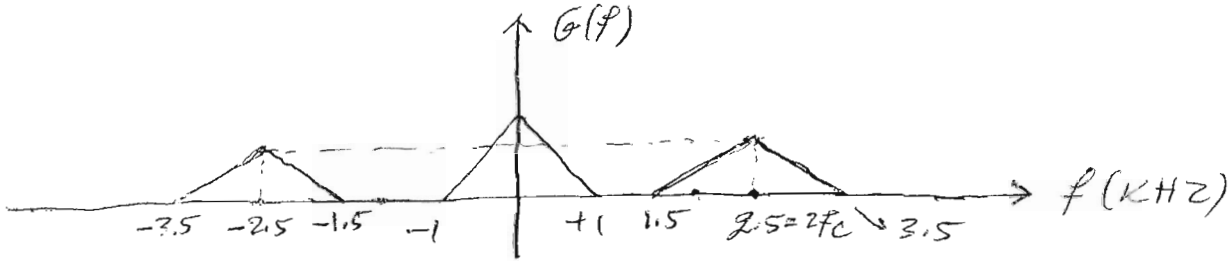
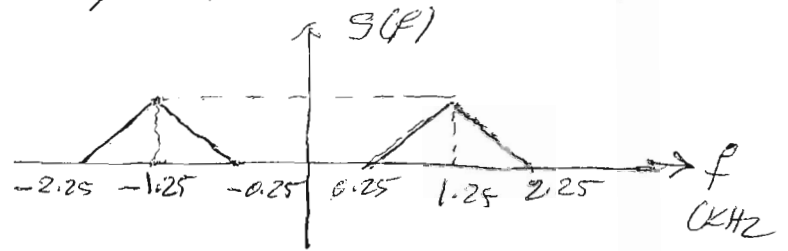
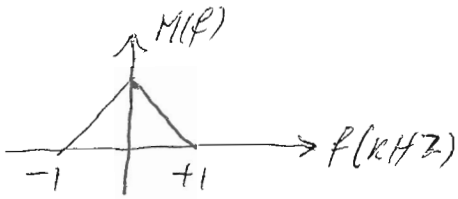
fig # (2) Coherent detection of DSB-SC.

$$y(t) = m(t) c(t) = A_c m(t) \cos 2\pi f_c t \Rightarrow S_y(f) = \frac{A_c}{2} [M(f-f_c) + M(f+f_c)] \quad (1)$$

$$g(t) = y(t) \cdot c'(t) = A_c A_c' m(t) \cos^2 2\pi f_c t = \frac{A_c A_c'}{2} m(t) [1 + \cos 4\pi f_c t] \quad (2)$$

$$G(f) = \frac{A_c A_c'}{2} M(f) + \frac{A_c A_c'}{4} [M(f-2f_c) + M(f+2f_c)] \quad (3)$$

a) For $f_c = 1.25$ kHz, the spectrum of $m(t)$, the spectrum of $y(t)$ and the spectrum of $v(t)$ (detector output) are:



b) For $f_c = 0.75$ KHz, the respective spectra are :

